

Material-Modeling Support for PFC

David Potyondy

Originally: Itasca Webinar (December 14, 2017)
Updated for fistPkg26, fistPkg6.6, fistPkg{7.1, 7.2, 7.3}
June 29, 2023

Preamble

• BPM methodology is described in Potyondy (2015), it will be briefly described in this webinar.

Potyondy, D.O. (2015) "The Bonded-Particle Model as a Tool for Rock Mechanics Research and Application: Current Trends and Future Directions," *Geosystem Engineering*, 18(1), 1–28.

Preamble

• Material-Modeling Support package is described in Potyondy (2017), and is the focus of this webinar.

Potyondy, D. (2017) "Material-Modeling Support in PFC [fistPkg25]," Itasca Consulting Group, Inc., Technical Memorandum ICG7766-L (March 16, 2017), Minneapolis, Minnesota.

*Operates within *PFC*, see Material Modeling Support link: www.itascacg.com/material-modelling-support.

fistPkg for PFC version 7 is fistPkg7.N, where N is package version number

Potyondy, D. (2023) "Material-Modeling Support in PFC [fistPkg7.3]," Itasca Consulting Group, Inc., Technical Memorandum ICG7766-L (June 29, 2023), Minneapolis, Minnesota.

Preamble

• Future webinars will introduce the BPM methodology, and discuss how to calibrate a BPM to match behavior of a particular rock.

For now, calibration notes:

Potyondy, D. (2018) "Calibration of the Flat-Jointed Material," PowerPoint Slide Set (April 13, 2018).

Questions?

- The large number of webinar attendees makes it impossible for me to reply to questions on-the-fly.
- However, you can submit your questions during the webinar using the chat-tool, or send them to Judy Zetterlund < jzetterlund@itascacg.com >.
- All questions will be answered, and the answers will be posted to the Itasca website within two weeks. This webinar will also be posted to the Itasca website. A link to the materials will be sent to all registrants.

Overview

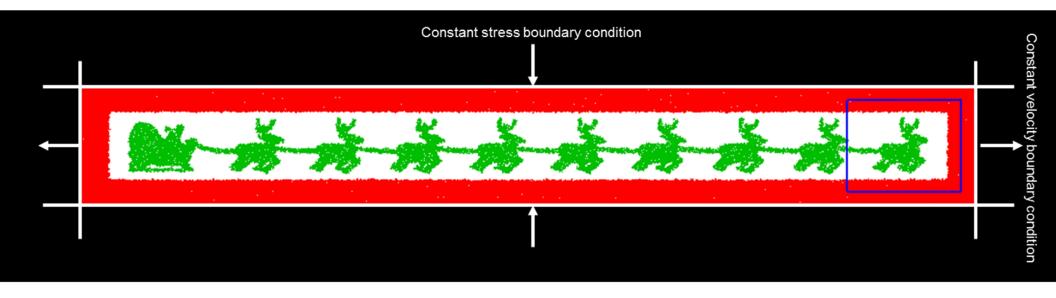
Bonded-Particle Modeling (Essential Features)

Material-Modeling Support Package (Walk-Through, lecture)



Material-Modeling Support Package (Hands-On, usage)

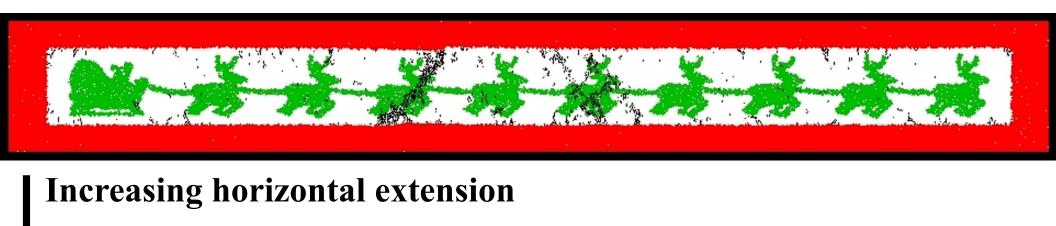
Bonded-Particle Modeling (Essential Features)

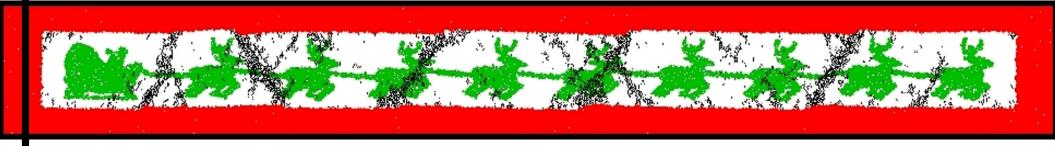


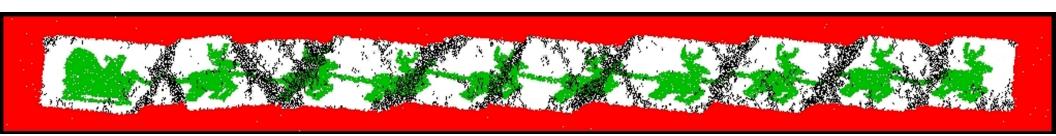
From Martin Schöpfer

Structural-geology application

Bonded-Particle Modeling (Essential Features)







Bonded-Particle Modeling (Essential Features)

6

Evolution of layer-bound fault systems

Fault systems occur on a wide range of scales (km to mm) and exhibit a wide range of geometries, ranging from symmetric (i.e. equal proportions of 'right' and 'left' dipping faults) to asymmetric (all faults dip in one direction). Asymmetric fault systems are often interpreted to form due to layer parallel shearing (e.g. domino or bookshelf-type faulting). 2D DEM models of fault systems under co-axial strain boundary conditions reveal that this interpretation may sometimes be incorrect.

Symmetric fault system



Photo: B. Grasemann

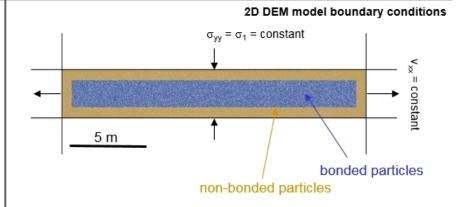
Quartzitic Marble, Serifos, Greece

Asymmetric fault system



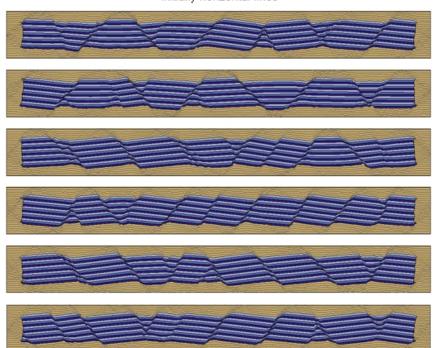
Photo: B. Grasemann

Pegmatitic dyke in marble, Naxos, Greece

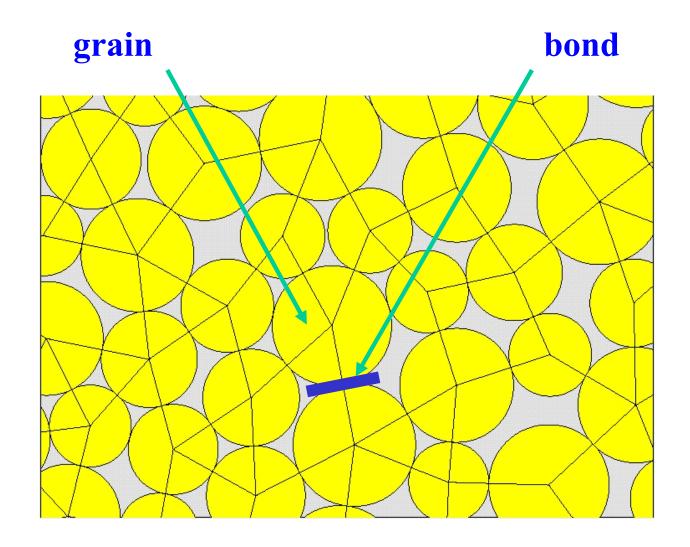


Six realisations at 10% extension

Passive markers obtained by intersecting triangulation of particle centres with
initially horizontal lines



Essential Features of a BPM



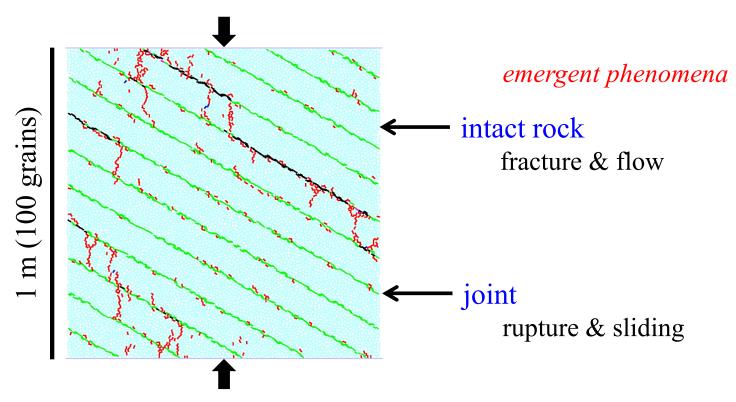
Damage consists of bond breakages.

Essential Features of a BPM

BPM consists of a base material (intact rock) to which larger-scale joints can be added.

• base material: bonded rigid grains

• joints : interfaces

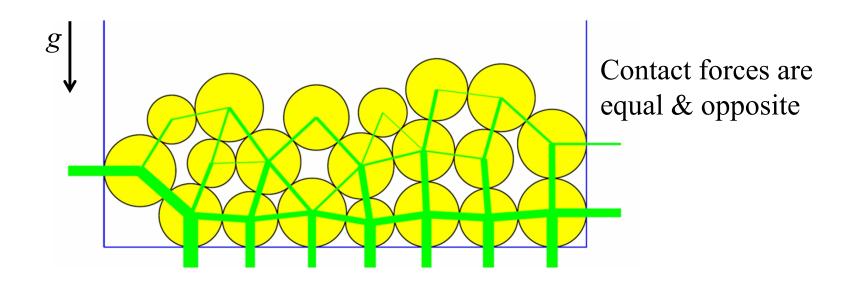


Damage consists of bond breakages.

Bonded-Particle Modeling Methodology (PFC model)

PFC programs (PFC2D & PFC3D) provide a general-purpose, distinct-element modeling framework that includes a computational engine and a graphical user interface.

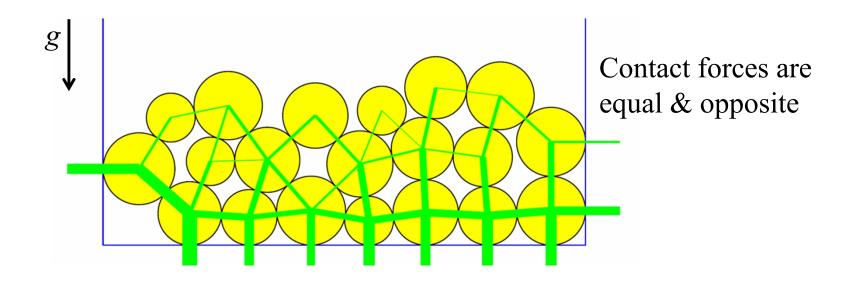
Simulate movement & interaction of many finite-sized particles via distinct-element method, which provides an explicit dynamic solution to Newton's laws of motion.



Bonded-Particle Modeling Methodology (PFC model)

Particles are rigid bodies with finite mass that move independently of one another and can both translate and rotate. Particles interact at pair-wise contacts by means of internal force and moment.

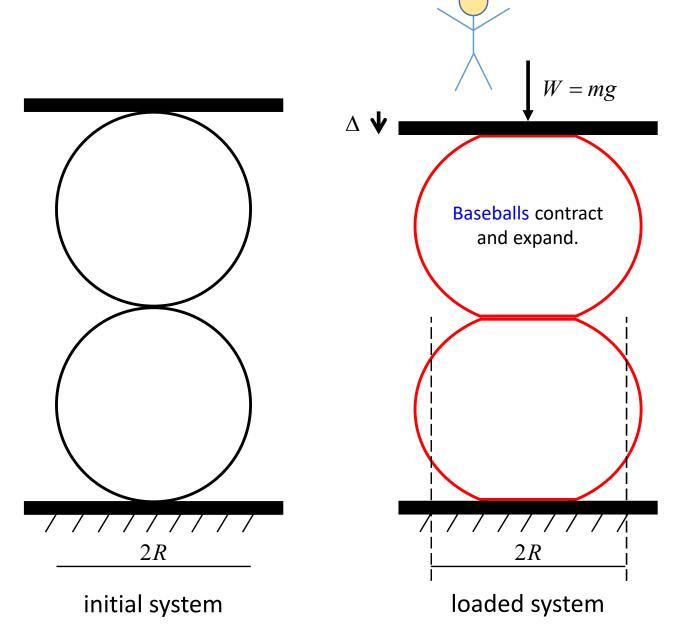
Contact mechanics is embodied in particle-interaction laws that employ a soft-contact approach for which all deformation occurs at the contacts between the rigid bodies. The particle-interaction law (contact model) updates the internal force and moment.



soft-contact approach

Consider the system of me standing on two baseballs, pressed between steel plates.

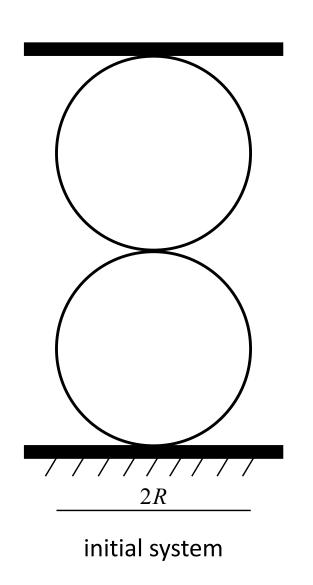
Top plate moves down by Δ .

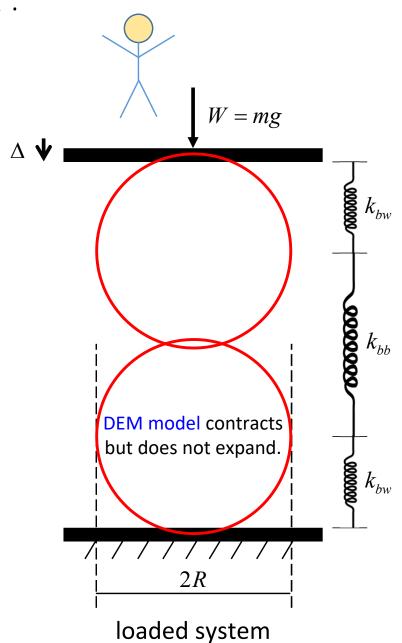


soft-contact approach

Consider the system of me standing on two baseballs, pressed between steel plates.

Top plate moves down by Δ .





DEM model employs a "soft contact" approach:

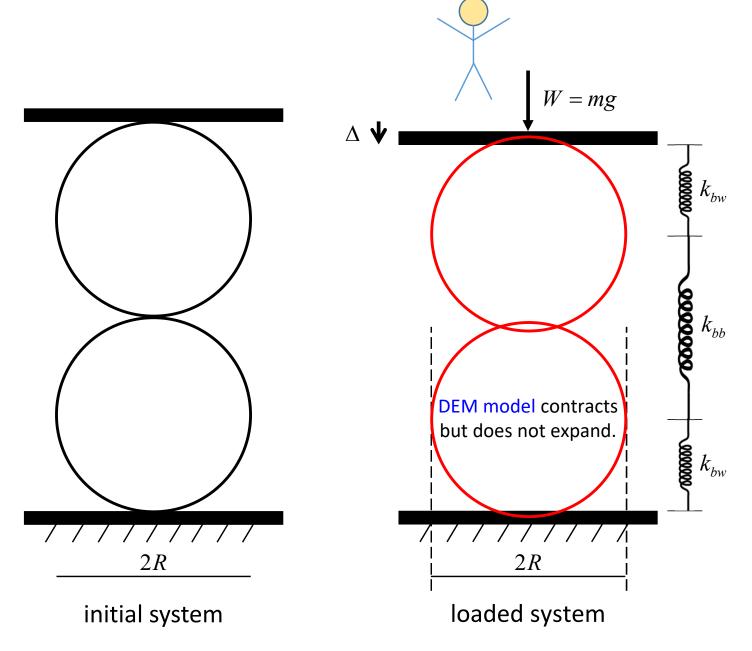
all deformation occurs at the contacts between the rigid bodies.

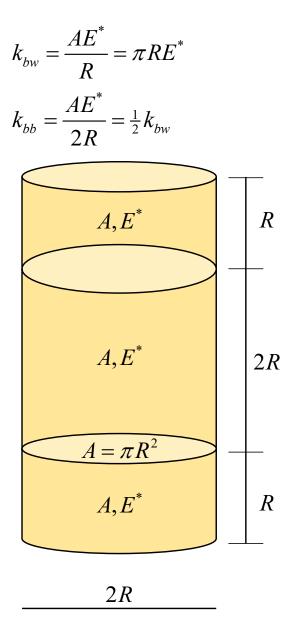
The stiffnesses can be related to the effective modulus of an equivalent continuum. . .

soft-contact approach

Consider the system of me standing on two baseballs, pressed between steel plates.

Top plate moves down by Δ .





equivalent continuum

Bonded-Particle Modeling Methodology (PFC model)

PFC model provides three basic entities:

balls and clumps

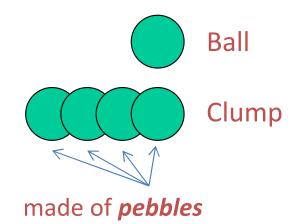
- obey laws of motion
- interact with one another and with walls

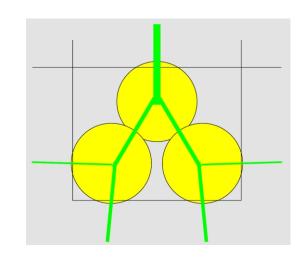
walls

- do not obey laws of motion
- used to apply velocity boundary conditions
- interact *only* with balls and clumps
- made of facets

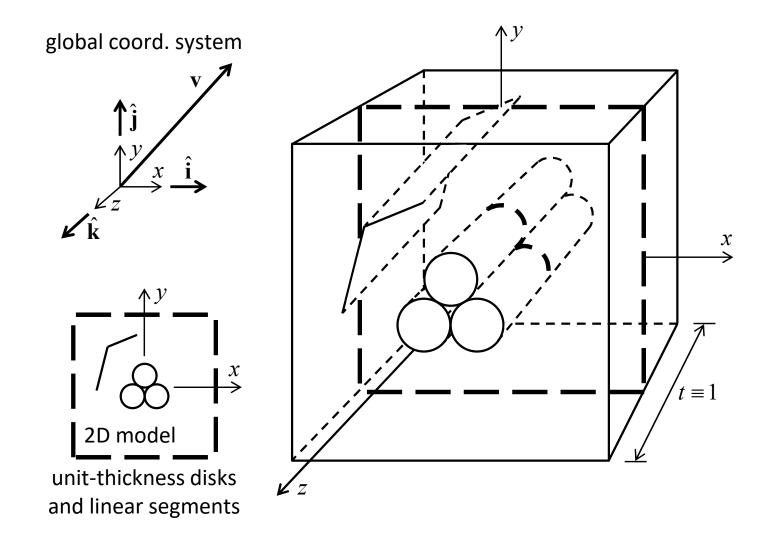
These entities interact at contacts.

Each contact stores force & moment that act on the two contacting entities.





Bonded-Particle Modeling Methodology (PFC model, 2D)



PFC2D model: unit-thickness disks and linear segments

Bonded-Particle Modeling Methodology (PFC model)

PFC model provides a synthetic material: rigid grains that interact at contacts, which encompasses a vast microstructural space --- only a small portion of this space has been explored.

PFC model includes both granular and bonded materials as well as an interface that can be inserted into the bonded materials.

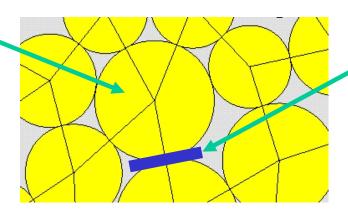
The most up-to-date incarnation of the PFC model is provided in the form of the linear, contact-bonded, parallel-bonded, and flatjointed materials to support:

- practical applications (via boundary-value models made from them)
- scientific inquiry (via further exploration of microstructural space)

Microstructural Models Provided by BPM

Base material itself can serve as model of intact rock

• rigid grains joined by deformable & breakable cement



grains can be balls, clumps or rigid blocks

cement can be

- contact-bonded contact
- parallel-bonded contact
- flat-jointed contact

Also soft-bonded &

subspring network contacts

When bond breaks, behaves as linear contact.

cement can be

- contact-bonded contact
- Also soft-bonded & subspring network contacts
- parallel-bonded contact
- flat-joint contact

When bond breaks, behaves as linear contact.

It is the type of contact model at the grain-grain contacts that defines the PFC material as being linear, contact-bonded, parallel-bonded, soft-bonded, flat-jointed or SNed.

Each material is defined by a set of material properties. These properties control the material-genesis procedure, install the desired contact model at selected contacts and assign contact-model properties.

Let's examine each contact model.

Linear Model

Linear Contact Bond Model

No time, future webinar!

Linear Parallel Bond Model & Soft Bond Model

Flat-Joint Model & Subspring Network Model



Material-Modeling Support Package (Walk-Through, lecture)



Material-Modeling Support Package (Hands-on, usage)

Let's begin...

Introduction

The PFC model provides a synthetic material consisting of an assembly of rigid grains that interact at contacts. This synthetic material encompasses a vast microstructural space, and only a small portion of this space has been explored.

The PFC model includes both granular and bonded materials. The bonded materials are also called Bonded-Particle Models (or BPMs).

The support for material modeling provided by PFC 5.0 consists of a consistent set of FISH functions, which we call the PFC 5.0 FISHTank (or fistPkg).

fistPkg for PFC version 7 is fistPkg7.N, where N is package version number

Overview of fistPkg

- Material Vessels & Material-Genesis Procedure
 - packing phase, then finalization phase
- Materials
 - common material properties
 - specific material properties (for each material type)
- Microstructural Monitoring
- Laboratory-Testing Procedures
 - measuring stress-strain-porosity
 - compression, diametral compression & direct tension
- Example Materials

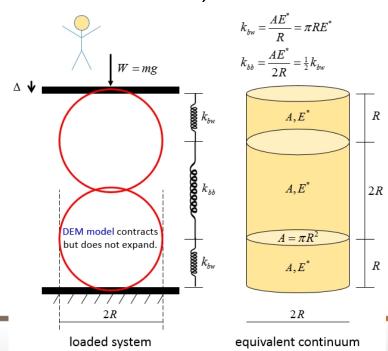
All materials are produced within a material vessel such that they form a homogeneous, isotropic and well-connected grain assembly with a specified non-zero material pressure.

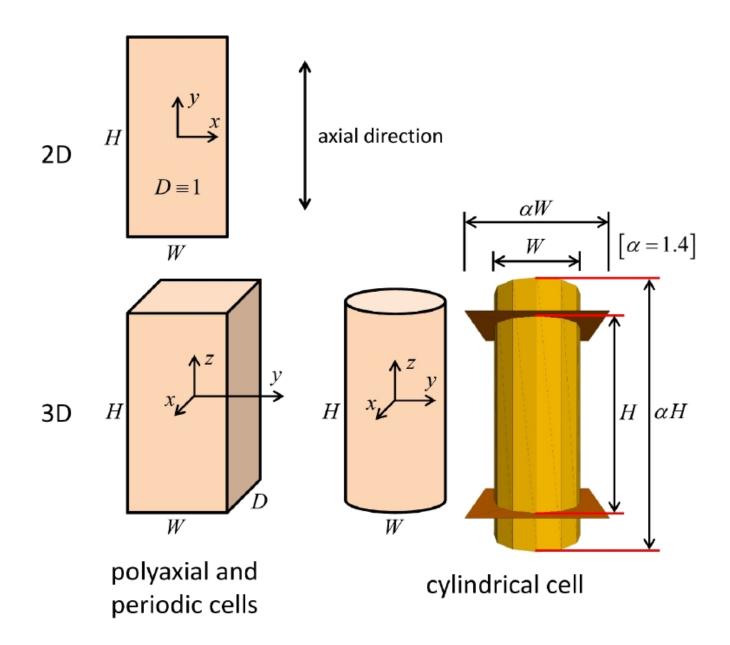
The linear contact model is installed at the grain-wall contacts. The walls are frictionless, and grain-wall contact stiffness is set based on a specified contact deformability (effective modulus).

All materials are produced within a material vessel such that they form a homogeneous, isotropic and well-connected grain assembly with a specified non-zero material pressure.

The linear contact model is installed at the grain-wall contacts. The walls are frictionless, and grain-wall contact stiffness is set based on a specified contact deformability (effective modulus).

Should be greater than or equal to modulus of the material.

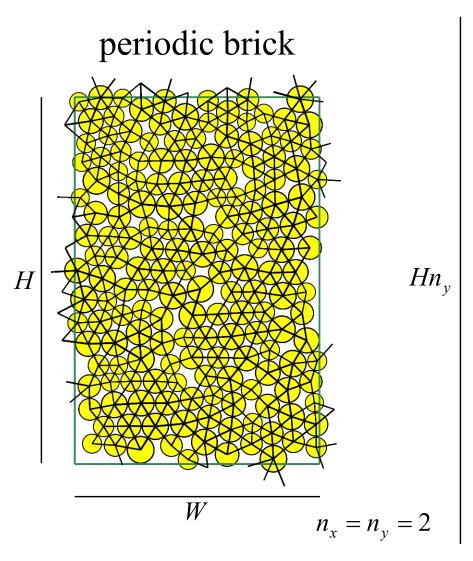


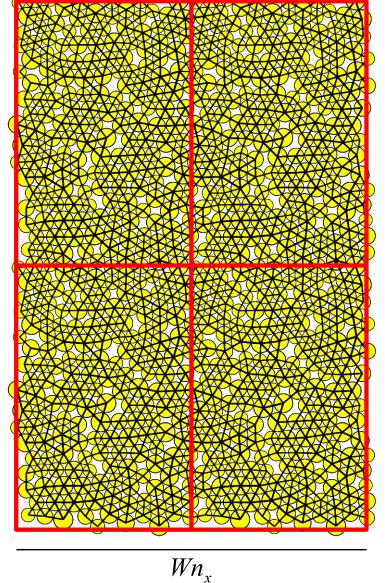


Material Vessels (periodic vessel)

Bricks are assembled into a perfectly packed ensemble, may have installed stress.

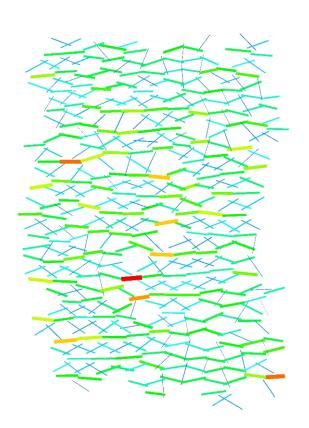
assembled specimen



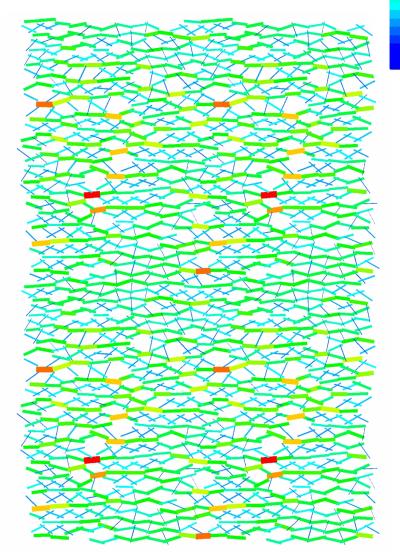


Material Vessels (periodic vessel)

Installed stress: Sxx = -78 MPa, Syy = -19.5 MPa



Force chains in bonded ensemble



Contact force_mag

Contacts (467)
2.0340E+5
1.9000E+5
1.7000E+5
1.5000E+5
1.3000E+5
1.1000E+5

9.0000E+4 7.0000E+4

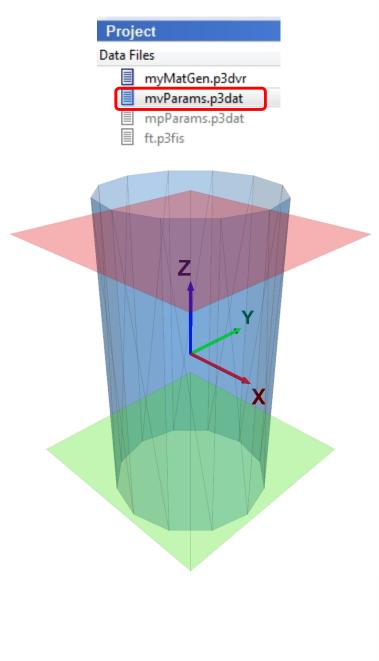
5.0000E+4 3.0000E+4

1.0000E+4

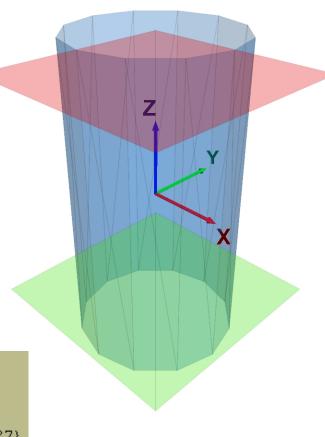
5.5113E+3

Table 6 Material-Vessel Parameters

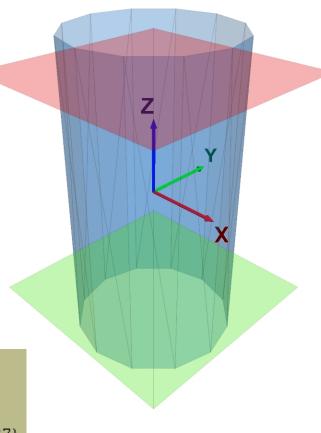
Parameter, FISH	Туре	Range	Default	Description
Material-vessel properties (including current vessel dimensions) are listed via @mvListProps.				
$T_{\!\scriptscriptstyle V}$, $\mathtt{mv_type}$	INT	{0,1}	0	vessel-type code { 0, physical 1, periodic
$S_{\!\scriptscriptstyle V}$, ${ m mv_shape}$	INT	{0,1,2}	0	vessel-shape code $\begin{cases} 0, & \text{rectangular cuboid} \\ 1, & \text{cylinder} \\ 2, & \text{sphere} \end{cases}$ (2D model: $S_{\nu} \equiv 0$)
{H,W,D}, mv_{H,W,D}		$(0.0,\infty)$ $[1.0,\infty)$		height, width and depth (sphere diameter is H ; 2D model: $D \equiv 1$, see Figure 2) expansion factor
$lpha$, \mathtt{mv} _expandFac $\{lpha_{\!\scriptscriptstyle I},lpha_{\!\scriptscriptstyle d}\}$,	FLI	[1.0,∞)	1.2	of physical vessel
$\{lpha_l,lpha_d\}$, mv_inset{L,D}Fac	FLT	(0.0,1.0]	{0.8,0.8}	inset factors of measurement regions
$E_{\!\scriptscriptstyle u}^{st}$, ${f mv}$ _emod	FLT	$\big(0.0,\infty\big)$	NA	effective modulus of physical vessel



```
Edit mvParams.p3dat*
 ;fname: mvParams.p3dat
def mvSetParams
 ; Set Material-Vessel Parameters.
 ; ** Cylindrical vessel (of 240-mm height and 170-mm diameter,
 ; ** with a 500 MPa effective modulus).
   mv type = 0
   mv shape = 1
   mv H = 240e-3
   mv W = 170e-3
   mv emod = 500e6
 end
 @mvSetParams
 @ mvCheckParams
 @mvListProps
 @msBoxDefine( [vector(0.0, 0.0, 0.0)], [vector(50e-3, 50e-3, 50e-3)] )
 return
 ;EOF: mvParams.p3dat
pfc3d>@mvListProps
## Material-Vessel Properties:
    mv type: 0 (physical)
    mv shape: 1 (cylinder, mvCylRes: 0.55)
    {mv H, wdz} (height {initial, current}, aligned with z-axis): {0.24,0.220127}
    {mv W, wdr} (diameter {initial, current}, lies in xy-plane): {0.17,0.152297}
    mv expandFac: 1.2
    mv emod (effective modulus): 5e+08
    mv insetLFac (measurement region spanning-length factor): 0.8
    mv insetDFac (measurement region diameter factor): 0.8
```



```
Edit mvParams.p3dat*
 ;fname: mvParams.p3dat
■def mvSetParams
 ; Set Material-Vessel Parameters.
 ; ** Cylindrical vessel (of 240-mm height and 170-mm diameter,
 ; ** with a 500 MPa effective modulus).
   mv type = 0
   mv shape = 1
   mV H = 240e-3
                      SI units, for legends of plots
   mv_W = 170e-3
   mv_emod = 500e6
 end
 @mvSetParams
 @ mvCheckParams
 @mvListProps
 @msBoxDefine( [vector(0.0, 0.0, 0.0)], [vector(50e-3, 50e-3, 50e-3)] )
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    {mv W, wdr} (diameter {initial, current}, lies in xy-plane): {0.17,0.152297}
    mv expandFac: 1.2
    mv emod (effective modulus): 5e+08
    mv insetLFac (measurement region spanning-length factor): 0.8
    mv insetDFac (measurement region diameter factor): 0.8
```



ITASCA

```
Edit mvParams.p3dat*
 ;fname: mvParams.p3dat
■def mvSetParams
  : Set Material-Vessel Parameters.
 ; ** Cylindrical vessel (of 240-mm height and 170-mm diameter,
 ; ** with a 500 MPa effective modulus).
   mv type = 0
   mv shape = 1
   mV H = 240e-3
                      SI units, for legends of plots
   mv_W = 170e-3
   mv = mod = 500e6
 end
 @mvSetParams
 @ mvCheckParams
 @mvListProps
 @msBoxDefine( [vector(0.0, 0.0, 0.0)], [vector(50e-3, 50e-3, 50e-3)] )
 return
 ;EOF: mvParams.p3dat
pfc3d>@mvListProps
## Material-Vessel Properties:
    mv type: 0 (physical)
    mv shape: 1 (cylinder, mvCylRes: 0.55)
                                                                                        microstructural box
    {mv H, wdz} (height {initial, current}, aligned with z-axis): {0.24,0.220127}
    {mv W, wdr} (diameter {initial, current}, lies in xy-plane): {0.17,0.152297}
    mv expandFac: 1.2
    mv emod (effective modulus): 5e+08
    mv insetLFac (measurement region spanning-length factor): 0.8
    mv insetDFac (measurement region diameter factor): 0.8
```

Materials

Material consist of circular/spherical, Voronoi and tetrahedral grains joined by contact, parallel or flat-joint bonds. Current implementation of Voronoi and tetrahedral grains is limited to 3D flat-joint contacts. The spherical, Voronoi and tetrahedral grains are shown here and will not be discussed further in this slide set. Refer to Potyondy et al. (2020) for a material description.

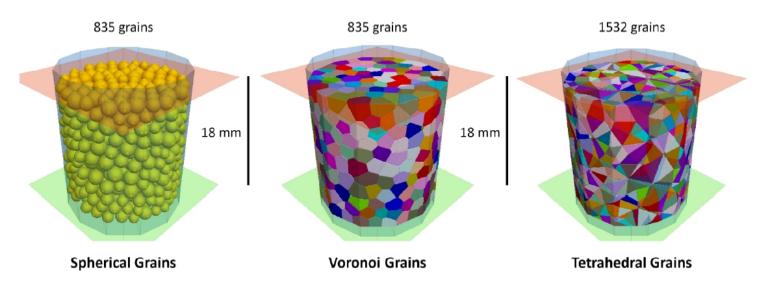


Figure 7 The three flat-jointed materials with spherical, Voronoi and tetrahedral grains at specimen resolutions of 10. (From Fig. 9 of Potyondy et al. [2020])

Material-Genesis Procedure (packing phase)

Generate cloud of grains drawn from specified size distribution at specified grain-cloud porosity. Allow them to rearrange into a packed state under conditions of zero friction. Then, obtain specified material pressure via:

boundary contraction:

move vessel walls under control of servomechanism [set $\mu = \mu_{CA}$, choose μ_{CA} to obtain dense or loose packing]

grain scaling:

grain sizes are scaled iteratively $[\mu \equiv 0 \text{ to obtain dense packing}]$

Material-Genesis Procedure (packing phase)

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[set $\mu = \mu_{CA}$, choose μ_{CA} to obtain dense or loose packing]

grain scaling:

grain sizes are scaled iteratively

[$\mu \equiv 0$ to obtain dense packing]

$$\mu_{CA} = 0 \text{ (dense)}$$

$$\mu_{CA} = \mu_m \text{ (loose)}$$

Table 7 Packing Parameters

Parameter	Туре	Range	Default	Description				
$S_{\scriptscriptstyle RN}$, ${ t pk}$ _seed	INT	$S_{RV} \ge 10,000$	10,000	seed of random-number generator (affects packing)				
$P_{\scriptscriptstyle m}$, ${ t pk_Pm}$	FLT	$\big(0.0,\infty\big)$	NA	material pressure				
$arepsilon_{_{P}}$, \mathtt{pk} _PTol	FLT	$(0.0,\infty)$	1×10^{-2}	pressure tolerance $\left(\frac{\left P-P_{m}\right }{P_{m}} \le \varepsilon_{P}\right)$				
${oldsymbol{arepsilon}}_{ ext{lim}}$, ${ t pk_ARatLimit}$	FLT	$(0.0,\infty)$	8×10^{-3}	where P is current pressure equilibrium-ratio limit (parameter of ft_eq)				
$n_{ m lim}$, pk_stepLimit	INT	$[1,\infty)$	25000	step limit (parameter of ft_eq)				
C_p , $\mathtt{pk_procCode}$	INT	{0,1}	0	packing-procedure code [0, boundary contraction				
$n_c^{}$, ${f pk}_{f n}$ c	FLT	(0.0,1.0)	$\begin{cases} \begin{cases} 0.58, & 3D \\ 0.25, & 2D \end{cases}, & C_p = 0 \\ \begin{cases} 0.35, & 3D \\ 0.08, & 2D \end{cases}, & C_p = 1 \end{cases}$	grain-cloud porosity				
Boundary-contraction	Boundary-contraction group ($C_p = 0$):							
$\mu_{\scriptscriptstyle CA}$, pk_fricCA	FLT	$\big[0.0,\infty\big)$	0.0	material friction coefficient during confinement application				
$v_{ m lim}$, pk_vLimit	FLT	$\big(0.0,\infty\big)$	NA	servo velocity limit (see Table 9)				

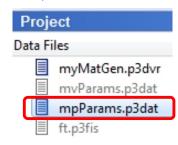
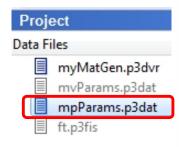


Table 7 Packing Parameters

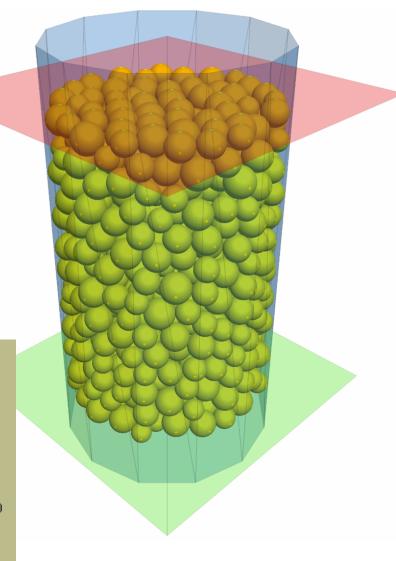
Parameter	Туре	Range	Default	Description
$S_{\scriptscriptstyle RN}$, ${f pk_seed}$	INT	$S_{RV} \ge 10,000$	10,000	seed of random-number generator (affects packing)
$P_{\scriptscriptstyle m}$, ${ t pk_Pm}$	FLT	$(0.0,\infty)$	NA	material pressure
$arepsilon_{_{P}}$, $\mathtt{pk_PTol}$	FLT	$(0.0,\infty)$	1×10^{-2}	pressure tolerance $\left(\frac{\left P-P_{m}\right }{P_{m}} \le \varepsilon_{P}\right)$
$arepsilon_{ ext{lim}}$, $ ext{pk_ARatLimit}$	FLT	$(0.0,\infty)$	8×10^{-3}	where P is current pressure equilibrium-ratio limit (parameter of ft_eq)
$n_{ m lim}$, ${ t pk_stepLimit}$	INT	$\big[1,\infty\big)$	25000	step limit (parameter of ft_eq)
$C_p^{}$, $\mathtt{pk_procCode}$	INT	{0,1}	0	packing-procedure code [0, boundary contraction] 1, grain scaling
n_c , ${f pk_nc}$	FLT	(0.0,1.0)	$\begin{cases} \begin{cases} 0.58, & 3D \\ 0.25, & 2D \end{cases}, & C_p = 0 \\ \begin{cases} 0.35, & 3D \\ 0.08, & 2D \end{cases}, & C_p = 1 \end{cases}$	grain-cloud porosity
Boundary-contraction	group	$(C_p = 0)$:		·
$\mu_{\scriptscriptstyle CA}$, pk_fricCA	FLT	$\big[0.0,\infty\big)$	0.0	material friction coefficient during confinement application
v _{lim} , pk_vLimit	FLT	$(0.0,\infty)$	NA	servo velocity limit (see Table 9)



pk_seed: affects particle arrangement

Edit mpParams.p3dat

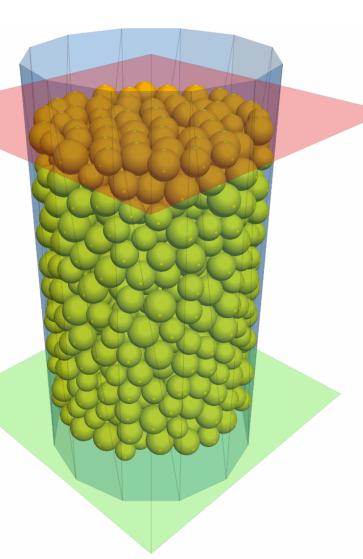
```
def mpSetPackingParams
; Set packing parameters.
   pk_Pm = 150.0e3
   pk_procCode = 0
   pk_nc = 0.58
   ; Boundary-contraction group:
        pk_fricCA = 0.0
        pk_vLimit = 1.0
end
@mpSetPackingParams
```



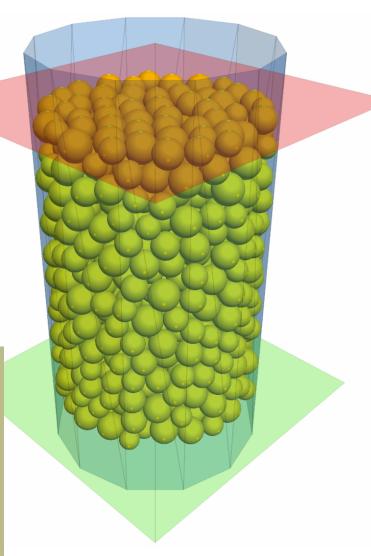
Edit mpParams.p3dat

```
def mpSetPackingParams
; Set packing parameters.
  pk_Pm = 150.0e3
  pk_procCode = 0
  pk_nc = 0.58
; Boundary-contraction group:
    pk_fricCA = 0.0
    pk_vLimit = 1.0
end
@mpSetPackingParams
```

Other parameters have default values.



```
def mpSetPackingParams
; Set packing parameters.
  pk_Pm = 150.0e3
  pk_procCode = 0
  pk_nc = 0.58
; Boundary-contraction group:
  pk_fricCA = 0.0
  pk_vLimit = 1.0
end
@mpSetPackingParams
```



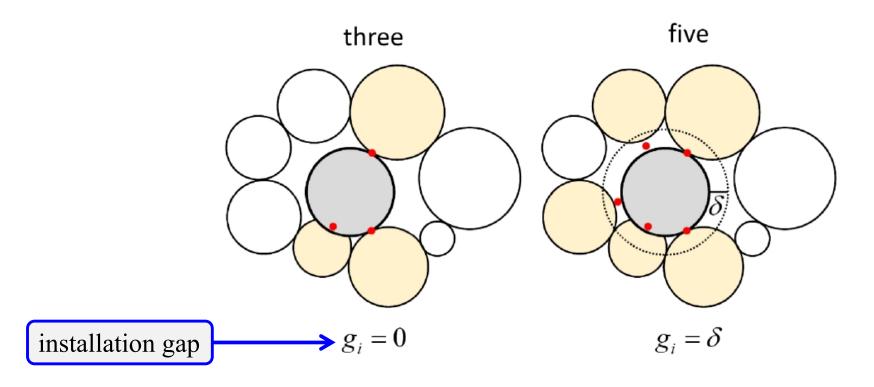
During the finalization phase:

- A. the final material properties are assigned to the grain-grain contacts, and
- B. additional material properties are specified that will be assigned to new contacts that may form during subsequent motion.

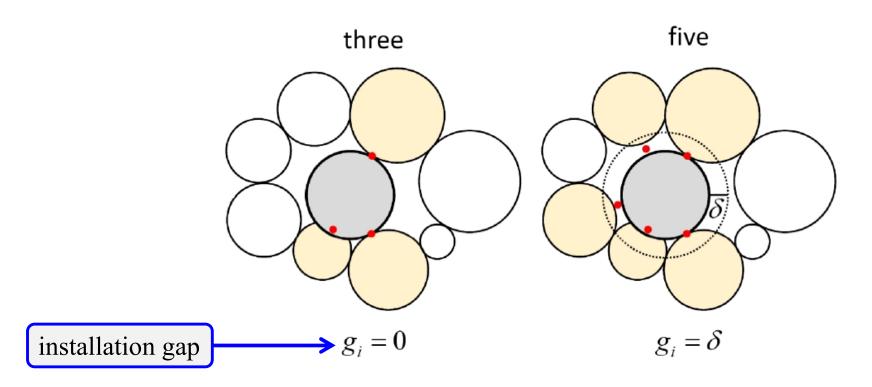
Table 3 Parallel-Bonded Material Parameters

	Parameter	Type	Range	Default	Description
	Common material	parameter	s are listed	in Table 1.	
	Packing paramete	rs are liste	d in Table 7		
	Parallel-bonded r	naterial gr	oup:		
	Linear group:				
A	• • •				
	Parallel-bond gro	up:			I
	• • •				
В	Linear material gr material finalization		rain-grain c	ontacts that n	nay form subsequent to

For the bonded materials, the installation gap controls the grain connectivity --- key parameter!

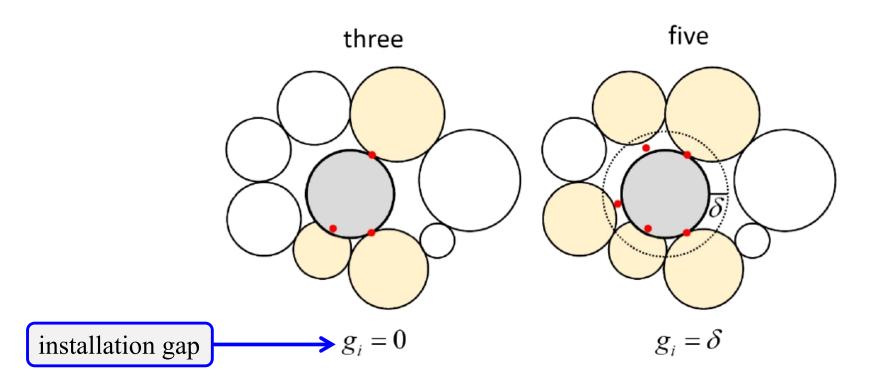


For the bonded materials, the installation gap controls the grain connectivity --- key parameter!



Increasing the installation gap, increases the grain connectivity.

For the bonded materials, the installation gap controls the grain connectivity --- key parameter!

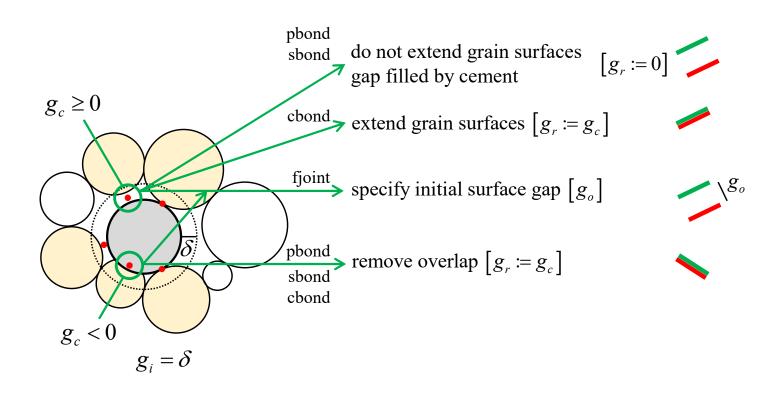


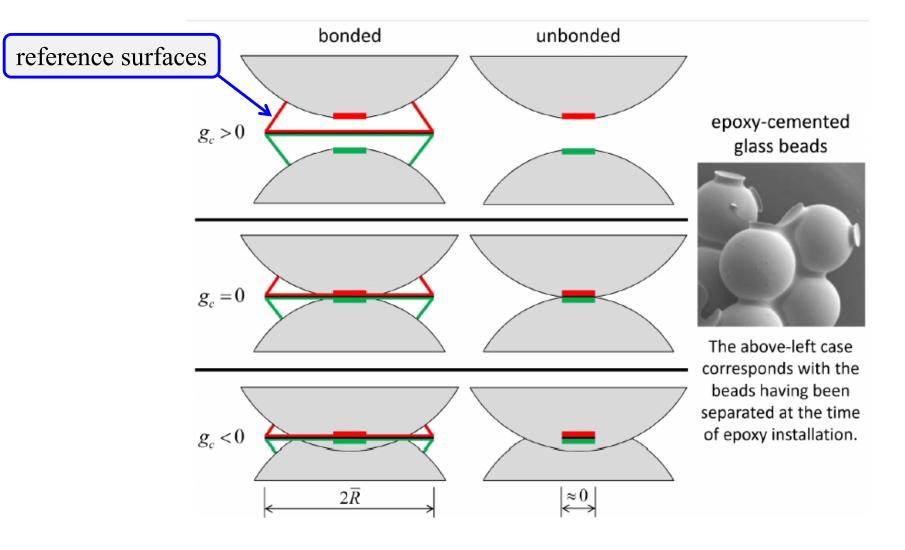
Increasing the installation gap, increases the grain connectivity,

which increases the material modulus and strength.

For the bonded materials, the material properties are set to establish reference surfaces that do not overlap.

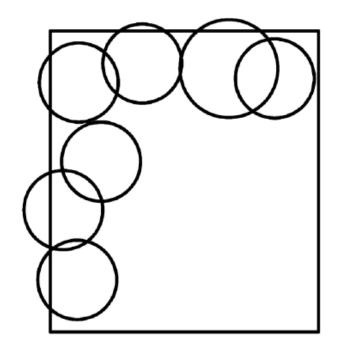
• There are no forces or moments in the material.



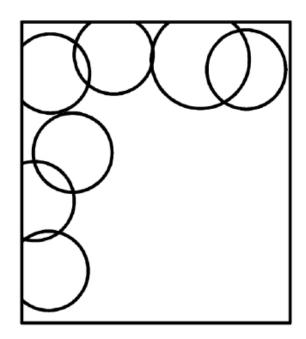


For the bonded materials, the grain-vessel interface is smoothed.

• There are no forces at the grain-wall interface.



Before smoothing

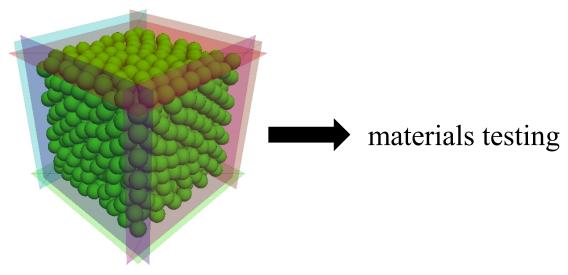


After smoothing

Material-Genesis Procedure (completed)

The specimen remains within the material vessel, and the model state

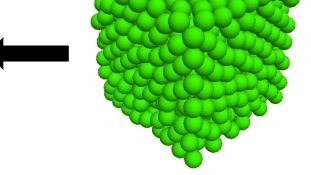
is saved.



For bonded materials, the specimen is removed from the material

vessel, and the model state is saved.

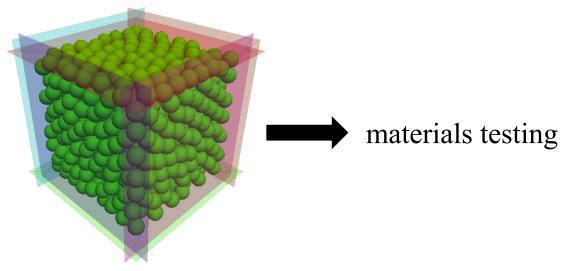
boundary-value simulation



Material-Genesis Procedure (completed)

The specimen remains within the material vessel, and the model state

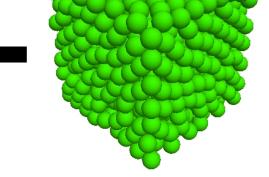
is saved.



For bonded materials, the specimen is removed from the material

vessel, and the model state is saved.

boundary-value simulation



The microstructural properties of the material are computed and listed by mpListMicroStrucProps and include the following items.

- Grain Size and Packing Information. Number of grains in the model, grain-size distribution (discussed below), average and median grain diameters, vessel resolutions w.r.t. the average and median grain diameters, ²⁵ measurement-based porosity (defined in Section 5.1), and overlap ratios. ²⁶
- Contact Information. The number of active linear-based contacts along with the number of such contacts that are grain-grain and grain-wall.
- Bonded-Material Information. The bonded materials provide this information. Bond coordination number (c_b) . ²⁷ Number of contact-bonded bonds, parallel-bonded bonds, softbonded bonds, flat-jointed contacts, flat-jointed elements, and flat-jointed bonds. The initial microstructural types of the flat-jointed material (defined in Section 2.7.2).

The microstructural properties of the material are computed and listed by mpListMicroStrucProps and include the following items.

- Grain Size and Packing Information. Number of grains in the model, grain-size distribution (discussed below), average and median grain diameters, vessel resolutions w.r.t. the average and median grain diameters, ²⁵ measurement-based porosity (defined in Section 5.1), and overlap ratios. ²⁶
- Contact Information. The number of active linear-based contacts along with the number of such contacts that are grain-grain and grain-wall.
- Bonded-Material Information. The bonded materials provide this information. Bond coordination number (c_b) . ²⁷ Number of contact-bonded bonds, parallel-bonded bonds, softbonded bonds, flat-jointed contacts, flat-jointed elements, and flat-jointed bonds. The initial microstructural types of the flat-jointed material (defined in Section 2.7.2).

Increasing the bond coordination number, increases the material modulus and strength.

Bond coordination number is increased by either: increasing the material pressure, or increasing the installation gap.

granular material

```
pfc3d>@mpListMicroStrucProps
## Material Microstructural Properties [# is "number of"]:
  Grain Size and Packing Information:
    mp nGN (# grains): 835
    Grain-size distribution (GSD) via gsdMeasure(numBins) to create table GSD,
      which is displayed in view pl-GSD.
                          (average grain diameter): 0.0170003
    mp Davg
    mp D50
                          ( median grain diameter): 0.0178
    mp PhiVavg (vessel resolution w.r.t. mp Davg ): 9.99983
    mp PhiV50 (vessel resolution w.r.t. mp D50 ): 9.55059
    mv mn (measurement-based porosity): 0.382552
    mp ORs (overlap ratios {max, min, avg}): {0.00211051,5.38026e-07,0.000554342}
  Contact Information:
    mp nLNc (# active linear-based
                                              contacts): 360
    mp nLNgg (# active linear-based grain-grain contacts): 0
    mp nLNgw (# active linear-based grain-wall contacts): 360
```

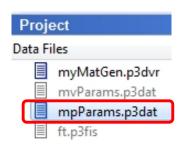
bonded material

```
pfc3d>@mpListMicroStrucProps
## Material Microstructural Properties [# is "number of"]:
   Grain Size and Packing Information:
    mp nGN (# grains): 1276
    Grain-size distribution (GSD) via gsdMeasure(numBins) to create table GSD,
      which is displayed in view pl-GSD.
    mp Davq
                          (average grain diameter): 0.00488862
                          ( median grain diameter): 0.00518062
    mp D50
    mp PhiVavg (vessel resolution w.r.t. mp Davg ): 10.2278
    mp PhiV50 (vessel resolution w.r.t. mp D50 ): 9.65135
    mv mn (measurement-based porosity): 0.303652
    mp ORs (overlap ratios {max, min, avg}): {0.0971667,1.12196e-05,0.019791}
   Contact Information:
    mp nLNc (# active linear-based
                                               contacts): 0
    mp nLNgg (# active linear-based grain-grain contacts): 0
    mp nLNgw (# active linear-based grain-wall contacts): 0
   Bonded-Material Information:
    mp CNb (bond coordination number via bcnMeasure): 6.60502
    mp nCBb (# contact-bonded bonds): 0
    mp nPBb (# parallel-bonded bonds): 0
    mp nSBb (# soft-bonded bonds): 4214
    mp nFJc (# flat-jointed contacts): 0
    mp nFJe (# flat-jointed elements): 0
    mp nFJb (# flat-jointed bonds): 0
```

Materials (common material properties)

Table 1 Common Parameters

Parameter	Type	Range	Default	Description
$N_{\it mt}$, cm_matName	STR	NA	PFCmat	material name (for model title)
$N_{\it ms}$, cm_matNameSAV	STR	NA	PFCmat	material name (for SAV file names)
T_m , cm_matType	INT	[0,5]	0	material-type code 0, linear 1, contact-bonded 2, parallel-bonded 3, soft-bonded 4, flat-jointed 5, user-defined
$N_{\it cm}$, cm_modName	STR	NA	NA	contact-model name ($T_m = 5$, also redefine ft setMatBehavior)
$lpha$, cm_localDampFac	FLT	[0.0, 0.7]	0.0	local-damping factor (for local damping)



Materials (common material properties)

$$C_p\,,\, {\tt cm_densityCode} \quad {\tt INT} \qquad \left\{0,1\right\} \qquad \quad 0$$

$$ho_{\!\scriptscriptstyle V}$$
 , cm_densityVal FLT $ig(0.0, \inftyig)$ NA

density code

density value (set grain density:

$$\rho_{g} = \begin{cases} \rho_{v}, C_{\rho} = 0 \\ \rho_{v}V_{v}/V_{g}, C_{\rho} = 1 \end{cases}$$

 $V_{\!\scriptscriptstyle \mathcal{V}}$ is volume of vessel, and

 $V_{\rm g}$ is total volume of grains)

myMatGen.p3dvr mvParams.p3dat mpParams.p3dat ft.p3fis

Project

Grain shape & size distribution group:

$$S_{g} \text{, cm_shape} \qquad \text{INT} \qquad \{0,1\} \qquad 0$$

$$n_{SD} \text{, cm_nSD} \qquad \text{INT} \qquad n_{SD} \geq 1 \qquad \text{NA}$$

$$T_{SD} \text{, cm_typeSD} (n_{SD}) \qquad \text{STR} \qquad \{0,1\} \qquad 0$$

$$N_{cl}^{(j)}, \text{ cm_ctName} (n_{SD}) \qquad \text{STR} \qquad \text{NA} \qquad \text{NA}$$

$$D_{l}^{(j)}, \text{ cm_Dlo} (n_{SD}) \qquad \text{FLT} \qquad (0.0, \infty) \qquad \text{NA}$$

$$D_{u}^{(j)}, \text{ cm_Dup} (n_{SD}) \qquad \text{FLT} \qquad D_{u}^{(j)} \geq D_{l}^{(j)} \qquad \text{NA}$$

$$\phi^{(j)}, \text{ cm_Dup} (n_{SD}) \qquad \text{FLT} \qquad (0.0, 1.0] \qquad \text{NA}$$

$$D_{mult}, \text{ cm_Dmult} \qquad \text{FLT} \qquad (0.0, \infty) \qquad 1.0$$

grain-shape code

1, all clumps

number of size distributions

size-distribution type

1, gaussian

clump-template name ($S_{\sigma} = 1$)

diameter range (lower)

diameter range (upper)

(clumps: volume-equiv. sphere)

volume fraction $\left(\sum \phi^{(j)} = 1.0\right)$

diameter multiplier

(shifts the size distribution)

Materials (common material properties)

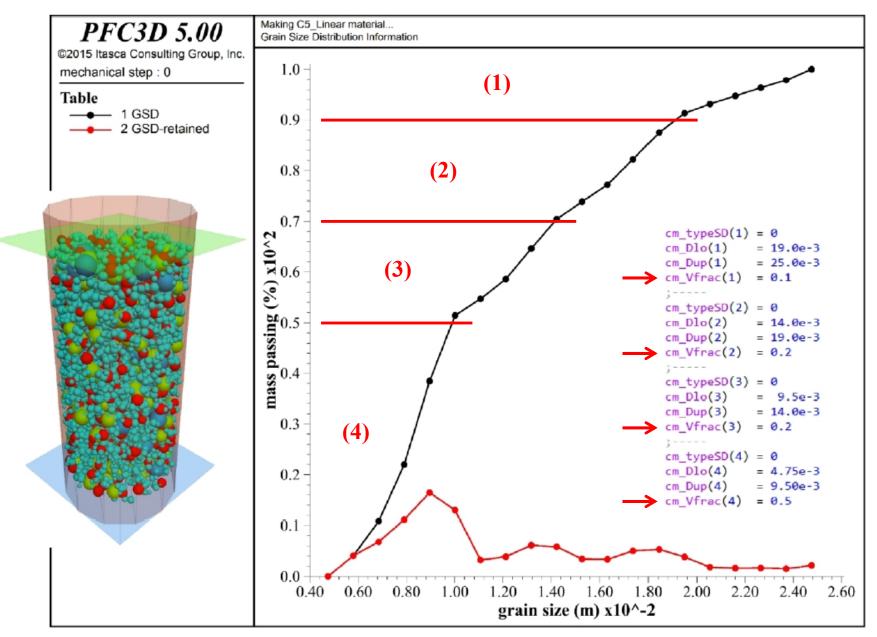
Edit mpParams.p3dat

```
■def mpSetCommonParams
 ; Set common parameters.
   cm matName = 'SS ContactBonded'
   ; ** Typical sandstone (contact-bonded material).
   cm_matType = 1
   cm localDampFac = 0.7
   cm densityCode = 1
   cm densityVal = 1960.0
   ; Grain shape & size distribution group:
     cm nSD = 1
     cm typeSD = array.create(cm nSD)
                                              pfc3d>@mpListMicroProps
     cm_ctName = array.create(cm_nSD)
                                              ## Material Microproperties:
     cm Dlo = array.create(cm nSD)
                                                 Common group:
     cm Dup = array.create(cm nSD)
                                                   cm matName (material name): SS ContactBonded
     cm_Vfrac = array.create(cm_nSD)
                                                   cm matType (material-type code): 1 (contact-bonded)
     cm_Dlo(1) = 4.0e-3
                                                   cm localDampFac (local-damping factor): 0.7
     cm Dup( 1) = 6.0e-3
                                                   cm densityCode: 1 (cm densityVal is bulk density)
                                                   cm densityVal: 1960
     cm_Vfrac(1) = 1.0
                                                   Grain shape & size distribution group:
 end
                                                     cm shape (grain-shape code): 0 (all balls)
 @mpSetCommonParams
                                                     cm nSD (number of size distributions): 1
                                                       cm typeSD(1): 0 (uniform)
                                                       cm Dlo(1): 0.004
                                                       cm Dup(1): 0.006
```

cm Dmult (diameter multiplier): 1

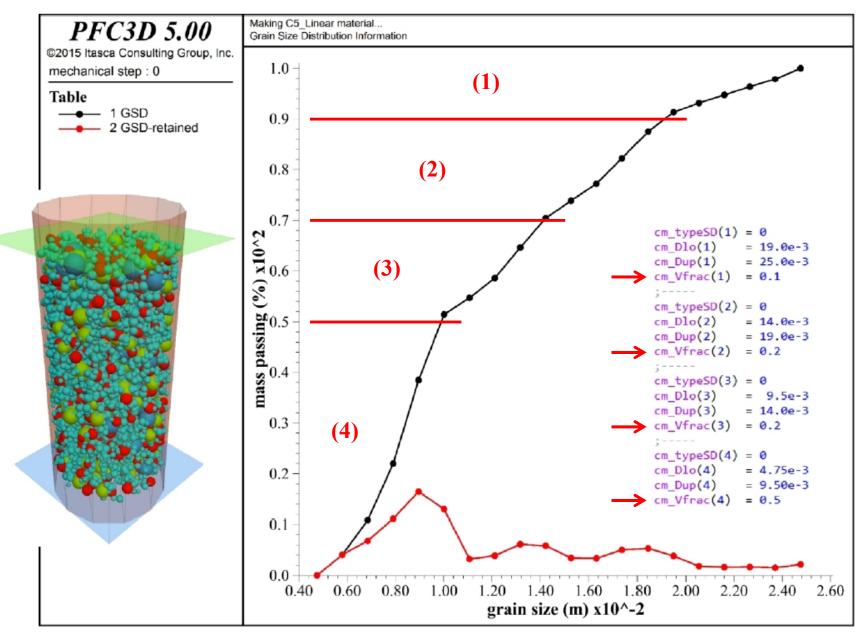
cm Vfrac(1): 1

Materials (grain-size distribution)



¹⁰ A given grain-size distribution (GSD) can be matched by specifying the volume fractions corresponding with the range of grain sizes — i.e., by breaking the given GSD into a finite number of uniform distributions (see Figure 14).

Materials (grain-size distribution)



A given grain-size distribution (GSD) can be matched by specifying the volume fractions corresponding with the range of grain sizes — i.e., by breaking the given GSD into a finite number of uniform distributions (see Figure 14).

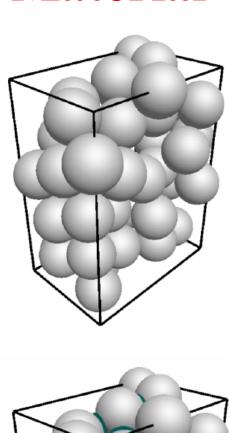
Microstructural Plot Sets

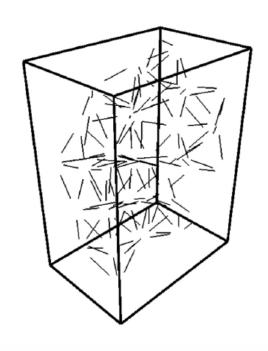
Microstructural plot sets are provided for the bonded materials to display the material microstructure and thereby reveal how the evolution of the microstructure influences the macroscopic behavior. The microstructural plot sets include depictions of the grains and the grain-grain interfaces, and when used with the crack-monitoring package, include the interface damage in the form of bond breakages.

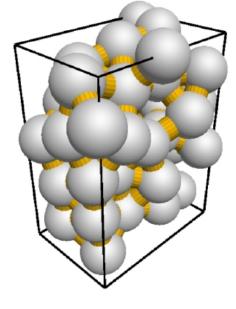
Figure image on next slide.

Figure 15 Microstructural plot sets for bonded materials with the same initial packing showing (clockwise from upper left): microstructural box and grains in the box (grey); contact-bonded material with contact bonds in the box; parallel-bonded material with parallel-bond cement (gold, 50% size) and parallel-bond interfaces (gold, 50% size); and flat-jointed material with flat-jointed interfaces (blue, 50% size).

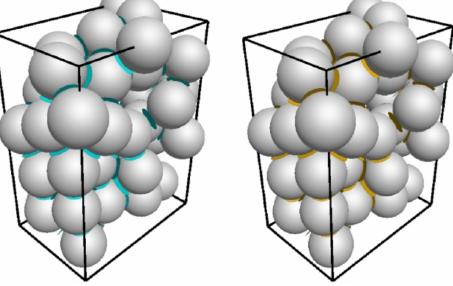
Material-Genesis (microstructural plot sets)

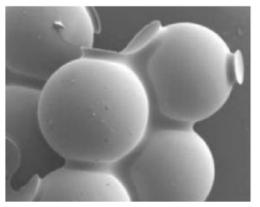




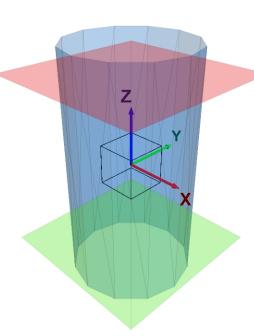


Glass beads cemented with epoxy





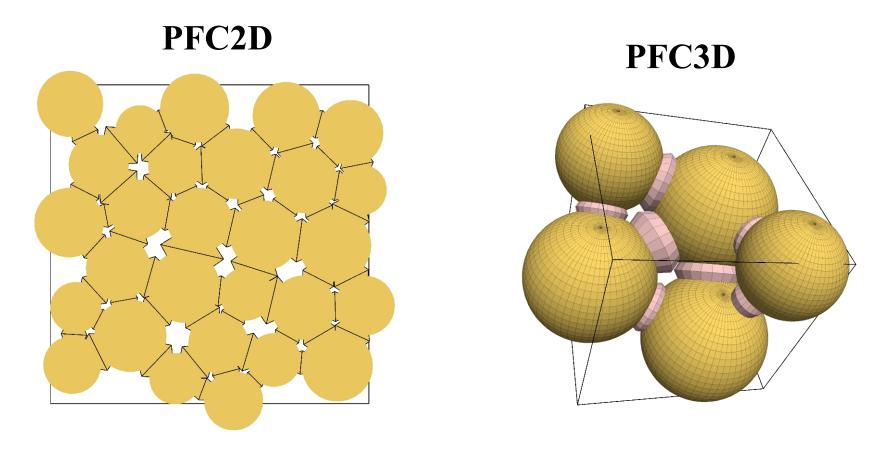
Holt et al. (2005)



microstructural box

Material-Genesis (microstructural plot sets)

Flat-jointed material, "faced grain" plot set



Grains in the microstructural box

Materials (linear material)

Table 2 Linear Material Parameters

Parameter	Type	Range	Default	Description

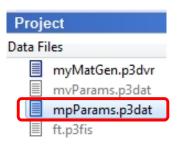
Material microproperties are listed via @mpListMicroProps.

Common material parameters are listed in Table 1.

Packing parameters are listed in Table 7.

Linear material group:

$$E^*$$
, lnm_emod FLT $\left[0.0,\infty\right)$ 0.0 effective modulus K^* , lnm_krat FLT $\left[0.0,\infty\right)$ 0.0 stiffness ratio μ , lnm_fric FLT $\left[0.0,\infty\right)$ 0.0 friction coefficient



```
\rightarrow (k_n, k_s)
```

Edit mpParams.p3dat*

```
50 □def mpSetLinParams
   ; Set linear material parameters.
52
      ; Common group (set in mpSetCommonParams)
53
      ; Packing group (set in mpSetPackingParams)
      ; Linear material group:
54
       lnm emod = 500e6
55
       lnm krat = 1.5
56
        lnm fric = 0.5
57
58
    end
   @mpSetLinParams
```

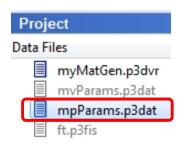
```
pfc3d>@mpListMicroProps
## Material Microproperties:
```

Linear material group: lnm_emod (effective modulus): 5e+08 lnm_krat (stiffness ratio): 1.5 lnm_fric (friction coefficient): 0.5

Materials (contact-bonded material)

Table 3 Contact-Bonded Material Parameters

Parameter	Type	Range	Default	Description				
Material micropropertie	Material microproperties are listed via @mpListMicroProps.							
Common material para	meters a	re listed in	Table 1.					
Packing parameters are	e listed in	Table 7.						
Contact-bonded mate	rial grou	ıp:						
Linear group:								
E^* , cbm_emod	FLT	$\left[0.0,\infty\right)$	0.0	effective modulus				
κ*, cbm_krat	FLT	$\left[0.0,\infty\right)$	0.0	stiffness ratio				
μ , cbm_fric	FLT	$[0.0,\infty)$	0.0	friction coefficient				



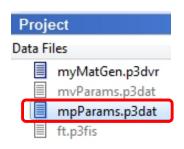
Materials (contact-bonded material)

Contact-bond group:				
$\overset{G}{S}$, cbm_igap	FLT	$\big[0.0,\infty\big)$	0.0	installation gap
$ig(T_{\sigma}ig)_{\{ ext{msd}\}}$ cbm_tens_{m,sd}	FLT	$[0.0, \infty)$	{0.0,0.0}	tensile-strength dist. [stress] (mean and std. deviation)
$\left(S_{\sigma}\right)_{\{ ext{msd}\}}$ cbm_shears_{m,sd}	FLT	$[0.0, \infty)$	{0.0,0.0}	shear-strength dist. [stress] (mean and std. deviation)
γ cbm_shearsTensRatio	FLT	$[0.0,\infty)$	0.0	(At each contact, set $S_{\sigma}=\gamma T_{\sigma}$. If $\gamma=0.0$, then $\left(S_{\sigma}\right)_{\{\!\!\text{msd}\!\!\}}$ is used.)
Linear material group (for subsequent to material final			ts during pa	cking and that may form
E_n^* , lnm_emod	FLT	$\left[0.0,\infty\right)$	0.0	effective modulus
$_{\mathcal{K}_{n}^{}^{*}}, \mathtt{lnm}\underline{\ }\mathtt{krat}$	FLT	$\left[0.0,\infty\right)$	0.0	stiffness ratio
$\mu_{n}, \mathtt{lnm_fric}$	FLT	$\left[0.0,\infty\right)$	0.0	friction coefficient

Materials (parallel-bonded material)

Table 4 Parallel-Bonded Material Parameters

Parameter	Type	Range	Default	Description				
Material microprope	Material microproperties are listed via @mpListMicroProps.							
Common material p	aramete	rs are listed	in Table 1.					
Packing parameters	s are liste	ed in Table 7						
Parallel-bonded m	aterial g	roup:						
Linear group:				_				
E^{st} , ${ t pbm_emod}$	FLT	$[0.0,\infty)$	0.0	effective modulus				
κ^* , pbm_krat	FLT	$[0.0,\infty)$	0.0	stiffness ratio				
μ , ${ t pbm_fric}$	FLT	$\big[0.0,\infty\big)$	0.0	friction coefficient				



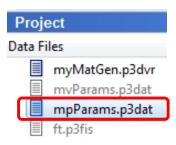
Materials (parallel-bonded material)

				,			
Parallel-bond group	:			-			
$g_{ m ,pbm_igap}$	FLT	$\big[0.0,\infty\big)$	0.0	installation gap			
$\overline{\lambda}$, pbm_rmul	FLT	$\big(0.0,\infty\big)$	1.0	radius multiplier			
$ar{\it E}^*$, pbm_bemod	FLT	$\big[0.0,\infty\big)$	0.0	bond effective modulus			
${ar \kappa}^*$, pbm_bkrat	FLT	$\big[0.0,\infty\big)$	1.0	bond stiffness ratio			
\overline{eta} , $ t pbm_{ar{}}$ mcf	FLT	$\begin{bmatrix} 0.0, 1.0 \end{bmatrix}$	0.0	moment-contribution factor			
$\left(ar{\sigma}_{\!\!c} ight)_{\!\!\{\!\! ext{msd}\!\!\}}$ pbm_ten_{m,sd}	FLT	$\big[0.0,\infty\big)$	{0.0,0.0}	tensile-strength dist. [stress] (mean and std. deviation)			
$\left(\overline{c}\right)_{\{m,sd\}}$ pbm_coh_{m,sd}	FLT	$\big[0.0,\infty\big)$	{0.0,0.0}	cohesion dist. [stress] (mean and std. deviation)			
$\overline{\gamma}$ pbm_cohTenRatio	FLT	[0.0,∞)	0.0	cohesion to tensile strength ratio (At each contact, set $\overline{c}=\overline{\gamma}\overline{\sigma}_{\!c}$. If $\overline{\gamma}=0.0$, then $(\overline{c})_{\!\{\!m,\!sd\!\}}$ is used.)			
$\overline{\phi}$, ${ t pbm_fa}$	FLT	[0.0, 90.0)	0.0	friction angle [degrees]			
_	Linear material group (for grain-grain contacts during packing and that may form subsequent to material finalization):						
E_{n}^{+} , lnm_emod	FLT	$\big[0.0,\infty\big)$	0.0	effective modulus			
κ_{n}^{*} , lnm_krat	FLT	$\big[0.0,\infty\big)$	0.0	stiffness ratio			
$\mu_{\!\scriptscriptstyle R}, { t lnm_fric}$	FLT	$\big[0.0,\infty\big)$	0.0	friction coefficient			

Materials (soft-bonded material)

Table 5 Soft-Bonded Material Parameters

Parameter	Туре	Range	Default	Description				
Material micropropert	Material microproperties are listed via @mpListMicroProps.							
·	Common material parameters are listed in Table 1.							
	Packing parameters are listed in Table 8.							
Sort-bonded materia	Soft-bonded material group:							
g_i , ${\tt sbm_igap}$	FLT	$[0.0,\infty)$	0.0	installation gap				
λ , sbm_rmul	FLT	$\big(0.0,\infty\big)$	1.0	radius multiplier				
E^* , ${\tt sbm_emod}$	FLT	$\big[0.0,\infty\big)$	0.0	effective modulus				
κ^* , sbm_krat	FLT	$\big[0.0,\infty\big)$	0.0	stiffness ratio				
eta , ${\tt sbm_mcf}$	FLT	$\begin{bmatrix} 0.0, 1.0 \end{bmatrix}$	0.0	moment-contribution factor				
$\left(\sigma_{c} ight)_{\{ ext{m,sd}\}}$ sbm_ten_{m,sd}	FLT	$\big[0.0,\infty\big)$	{0,0}	tensile-strength dist. [stress] (mean and std. deviation)				
$ (c)_{\{m,sd\}} $ $ sbm_coh_\{m,sd\} $	FLT	$\big[0.0,\infty\big)$	{0,0}	cohesion dist. [stress] (mean and std. deviation)				
γ	FLT	[0.0,∞)	0.0	(At each contact, set $c = \gamma \sigma_{\!c}$.				
sbm_cohTenRatio		[0.0,∞)	0.0	If $\gamma = 0.0$, then $\left(\mathcal{C}\right)_{\{\mathrm{m,sd}\}}$ is used.)				
ϕ , sbm_fa	FLT	[0.0,90.0)	0.0	friction angle [degrees]				
ζ , ${ t sbm_soft}$	FLT	$\big[0.0,\infty\big)$	0.0	softening factor ($\zeta = 0$ is no softening)				
γ , sbm_cut	FLT	[0.0,1.0]	0.0	strength-reduction factor ($\gamma = 0/1$ is full/no softening)				



Materials (soft-bonded material)

μ , ${\tt sbm_fric}$	FLT	$\left[0.0,\infty\right)$	0.0	friction coefficient (when unbonded)	
λ_b , sbm_bmul	FLT	$\left[0.0,\infty\right)$	0.0	bending-friction multiplier (when unbonded)	
λ_{t} , sbm_tmul	FLT	$\left[0.0,\infty\right)$	0.0	twisting-friction multiplier (when unbonded)	
Linear material group (for grain grain contacts during packing and that may form					

Linear material group (for grain-grain contacts during packing and that may form subsequent to material finalization):

$$E_n^*$$
, lnm_emod FLT $\left[0.0,\infty\right)$ 0.0 effective modulus κ_n^* , lnm_krat FLT $\left[0.0,\infty\right)$ 0.0 stiffness ratio μ_n , lnm_fric FLT $\left[0.0,\infty\right)$ 0.0 friction coefficient

Materials (flat-jointed material)

Table 6 Flat-Jointed Material Parameters

Parameter	Туре	Range	Default	Description		
Material microproperties are listed via @mpListMicroProps.						
Common material parameters are listed in Table 1.						
Packing parameters are list	ted in Tal	ole 8.				
Flat-jointed material grou	p:					
$C_{M\mathrm{S}}$, $\mathtt{fjm_trackMS}$	BOOL	{true, false}	false	microstructure-tracking flag (draw microstructure with the faced grain plot set)		
g_i , fjm_igap	FLT	$[0.0, \infty)$	0.0	installation gap		
$\phi_{_{\cal B}}^{^+}$, fjm_B_frac	FLT	[0.0,1.0]	NA	bonded fraction		
$\phi_{_{G}}^{^{+}}$, fjm_G_frac	FLT	[0.0,1.0]	NA	gapped fraction		
$(g_o)_{\{m,sd\}}$, fjm_G_{m,sd}	FLT	$\big[0.0,\infty\big)$	$\{0.0, 0.0\}$	initial surface-gap distribution (mean and std. deviation)		
_{N,} ,fjm_Nr	INT	[1,∞)	2	elements in radial direc. (2D model: total elements)		
$_{N_{_{\sigma}}}$, fjm_Nal	INT	[3,∞)	4	elements in circumf. direc. (3D model only)		
$C_{_{\! \lambda}}$, fjm_rmulCode	INT	{0,1,2}	0	radius-multiplier code $\begin{cases} 0, \ \lambda \text{ constant (no valid check)} \\ 1, \ \text{valid } (\lambda \text{ non-uniform reduce)} \\ 2, \ \text{valid } (\lambda \text{ uniform reduce)} \end{cases}$		
$\lambda_{_{\!ee}}$, fjm_rmulVal	FLT	(0.0,∞)	1.0	$ \begin{split} \text{radius-multiplier value} \\ \lambda &= \lambda_{_{\!$		
E , fjm_emod	FLT	[0.0,∞)	0.0	effective modulus		
κ^* , fjm_krat	FLT	$[0.0,\infty)$	0.0	stiffness ratio		

Project					
Data Files					
	myMatGen.p3dvr				
	mvParams.p3dat				
	mpParams.p3dat				
	ft.p3fis				

Materials (flat-jointed material)

μ , fjm_fric	FLT	$\big[0.0,\infty\big)$	0.0	friction coefficient		
$\left(\sigma_{c} ight)_{ ext{\{msd\}}}$ fjm_ten_{m,sd}	FLT	[0.0,∞)	{0.0, 0.0}	tensile-strength dist. [stress] (mean and std. deviation)		
$\left(\mathcal{C}\right)_{\{ ext{m,sd}\}}$ fjm_coh_{m,sd}	FLT	$\big[0.0,\infty\big)$	{0.0, 0.0}	cohesion dist. [stress] (mean and std. deviation)		
γ fjm_cohTenRatio	FLT	$[0.0,\infty)$	0.0	cohesion to tensile strength ratio (At each contact, set $c=\gamma\sigma_c$. If $\gamma=0.0$, then $\left(c\right)_{\{\text{msd}\}}$ is used.)		
\mathcal{C}_r fjm_cohres	FLT	$\big[0.0,\infty\big)$	0.0	residual cohesion [stress]		
$\boldsymbol{M_r}, \texttt{fjm_resmode}$	INT	$\big\{0,1\big\}$	0	shear-drop residual mode		
ϕ , fjm_fa	FLT	[0.0, 90.0)	0.0	friction angle [degrees]		
Linear material group (for grain-grain contacts during packing, that are not flat-jointed, and that may form subsequent to material finalization):						
E_n^* , lnm_emod	FLT	$\big[0.0,\infty\big)$	0.0	effective modulus		
${\kappa_n}^*, \mathtt{lnm_krat}$	FLT	$\big[0.0,\infty\big)$	0.0	stiffness ratio		
$\mu_{\!\scriptscriptstyle n}, { t lnm_fric}$	FLT	$\big[0.0,\infty\big)$	0.0	friction coefficient		

⁺ Slit fraction: $\phi_S = 1 - \phi_B - \phi_G \ \left(0 \le \phi_S \le 1\right)$.

Materials (flat-jointed material)

Microstructural Validity, valid if grain facets do not overlap

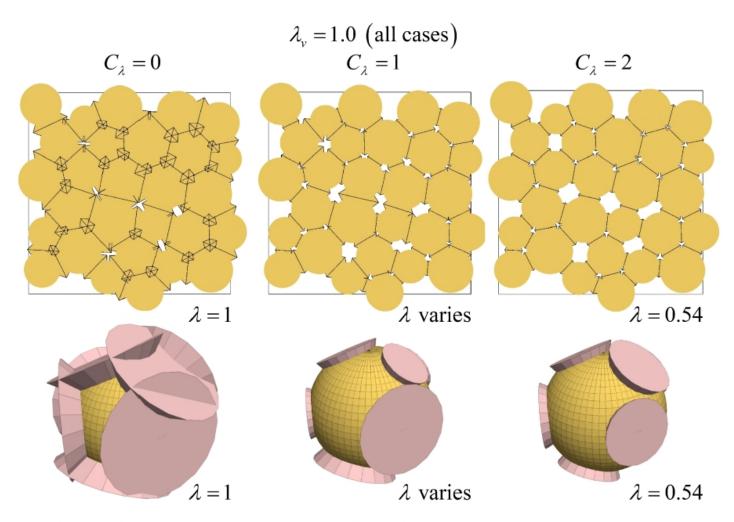
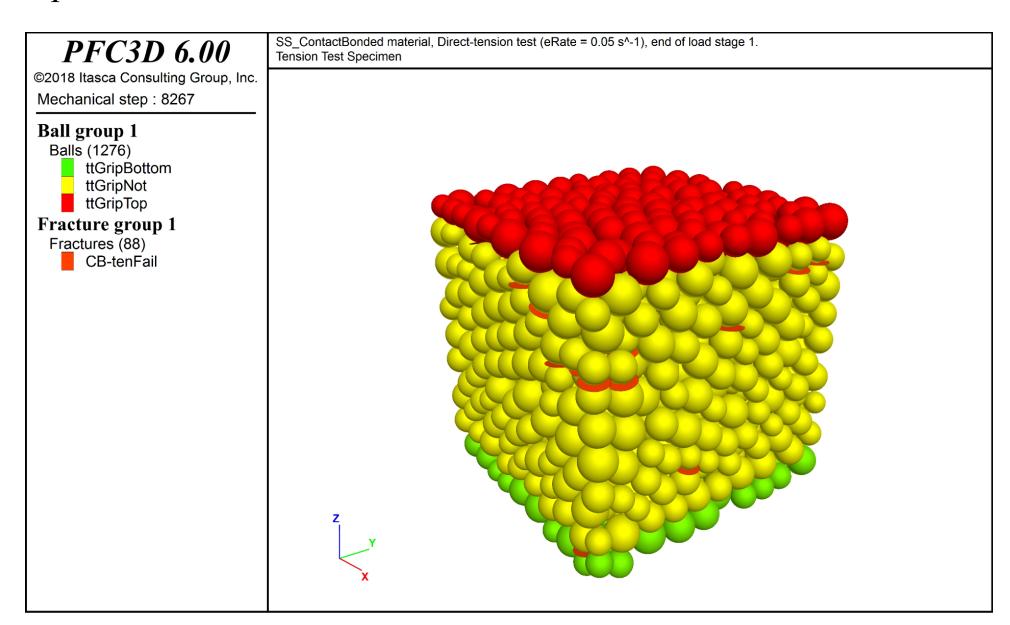


Figure 12 The three types of flat-jointed microstructures produced by the material-modeling support package. The left-most images have invalid microstructures, while the middle and right images have valid microstructures. Only a single faced grain is shown for the 3D case (bottom).

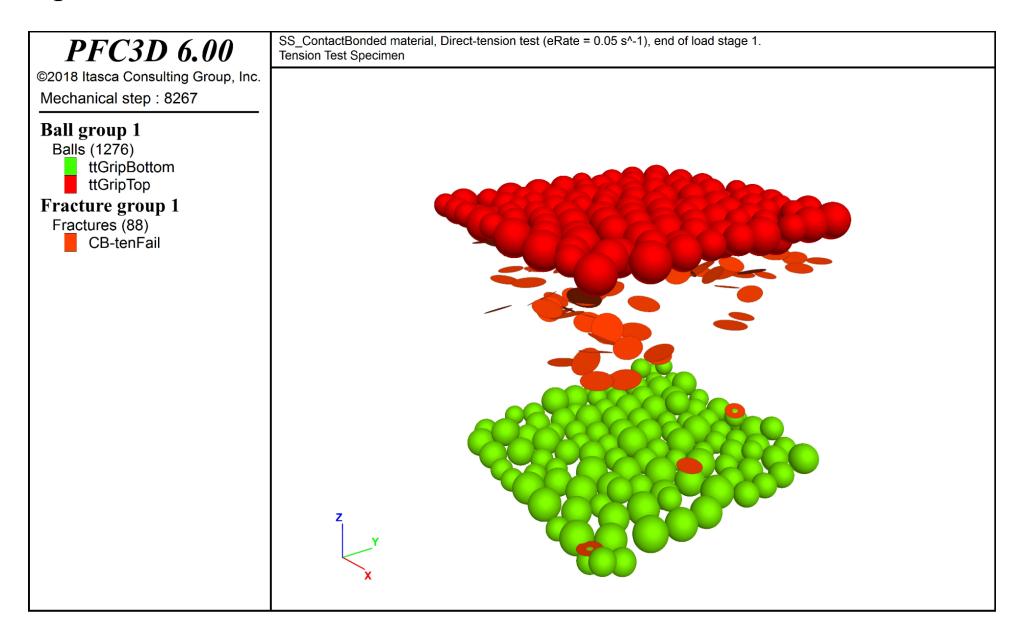
Damage in the bonded materials consists of bond breakages, which we denote as cracks. Crack data is stored as a Discrete Fracture Network (DFN), and the DFN plot item supports visualization of the cracks. Each crack has a type (contact bonded, parallel bonded, flat jointed or smooth jointed) and failure mode (tensile or shear).

The type and failure mode of all cracks are stored in the group name of the CrackData-DFN, and the numbers of these items are stored in the crack count global variables.

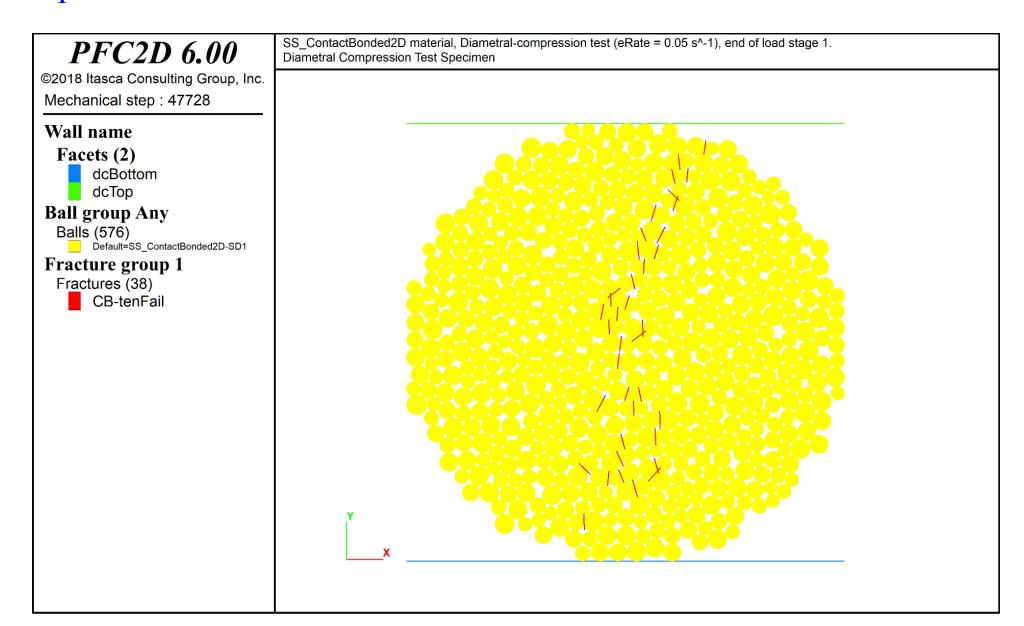
A crack is a disk for the 3D model and a segment of unit-thickness depth for the 2D model.



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"crack" plot set, displays cracks with thickness proportional to gap.

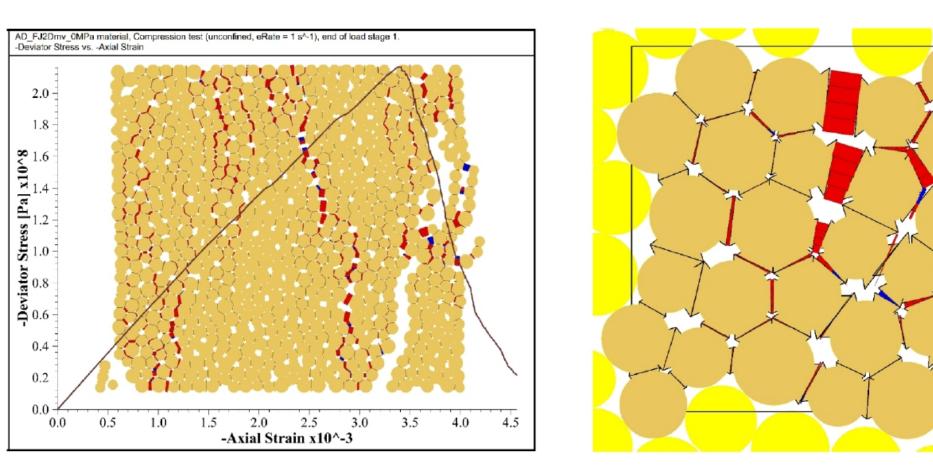


Figure 17 Crack and faced grain plot sets in 2D showing cracks, with crack thickness equal to gap, and cracks colored red/blue for tensile/shear failure. 2D flat-jointed material at end of UCS test as the specimen exhibits axial splitting.

"crack" plot set, displays cracks with thickness proportional to gap.

The right-most grain was moved to the right until all 16 flat-joint elements broke in tension. Then the inner grain was rotated causing the unbroken faces to break in shear.

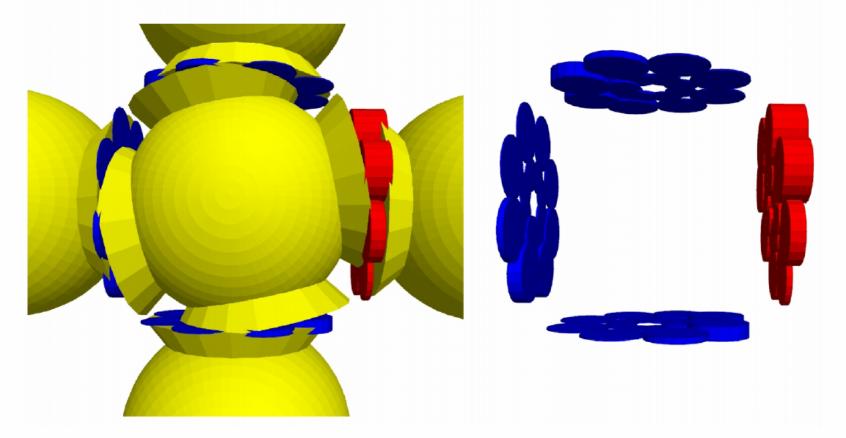
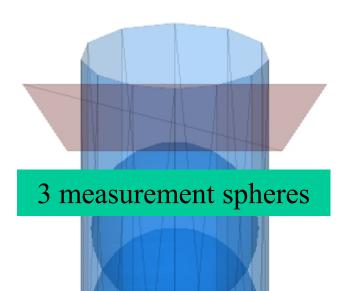


Figure 18 Crack and faced grain plot sets in 3D showing cracks, with crack thickness equal to gap, and cracks colored red/blue for tensile/shear failure.

Lab-Testing Procedures (stress-strain-porosity)

Table 8 Material-Vessel Stress, Strain and Porosity Quantities

Quantity, FISH	Description
$\left\{\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy}, \sigma_{xz}, \sigma_{yz}\right\},$ $mv_ms\{xx, yy, zz, xy, xz, yz\}$	material stress (2D model: $\sigma_{zz} \equiv \sigma_{xz} \equiv \sigma_{yz} \equiv 0$)
$\left\{\mathcal{E}_{xx}, \mathcal{E}_{yy}, \mathcal{E}_{zz}, \mathcal{E}_{xy}, \mathcal{E}_{xz}, \mathcal{E}_{yz}\right\},$ $mv_me\{xx, yy, zz, xy, xz, yz\}$	material strain (2D model: $\varepsilon_{zz} \equiv \varepsilon_{xz} \equiv \varepsilon_{yz} \equiv 0$)
$\left\{ oldsymbol{\sigma}_{\!a}, oldsymbol{\sigma}_{\!r} ight\}$, \mathtt{mv} _ms{a,r}	axial & radial stress
$\left\{ oldsymbol{arepsilon}_{a}, oldsymbol{arepsilon}_{r} ight\}$, mv_me{a,r}	axial & radial strain
$\sigma_{_d}$, \mathtt{mv} _msd	deviator stress
$\sigma_{_m}$, ${ t mv}_{oldsymbol{_}}{ t msm}$	mean stress
$arepsilon_{\!\scriptscriptstyle d}$, ${ t mv}_{\!$	deviator strain
$arepsilon_{_{\! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! \! $	volumetric strain
n, mv_mn	measurement-based porosity
$n_{_{\!\scriptscriptstyle{W}}}$, ${ t mv_wn}$	wall-based porosity





Lab-Testing Procedures (stress-strain-porosity)

We denote stress and strain by

stress:
$$\left\{\sigma_{xx}, \sigma_{yy}, \sigma_{zz}, \sigma_{xy}, \sigma_{xz}, \sigma_{yz}\right\}$$

strain: $\left\{\varepsilon_{xx}, \varepsilon_{yy}, \varepsilon_{zz}, \varepsilon_{xy}, \varepsilon_{xz}, \varepsilon_{yz}\right\}$ (4)

where $\sigma_{ii} > 0$ is tension and $\varepsilon_{ii} > 0$ is extension. For the 2D model, the out-of-plane stress and strain components are equal to zero so that stress is $\{\sigma_{xx}, \sigma_{yy}, \sigma_{xy}\}$ and strain is $\{\varepsilon_{xx}, \varepsilon_{yy}, \varepsilon_{xy}\}$.

The three measurement techniques measure the following quantities:

$$\sigma_{ij}^{m} \mathcal{E}_{ij}^{m}$$
 measurement-based (6 terms each, symmetric)
$$\sigma_{k}^{w} \mathcal{E}_{k}^{w}$$
 wall-based (3 terms each)
$$\mathcal{E}_{k}^{g}$$
 guage-based (3 terms)
$$\lim_{\substack{i,j=\{x,y,z\}\\k=\{x,y,z\}}} \mathcal{E}_{k}^{g}$$

Lab-Testing Procedures (summary)

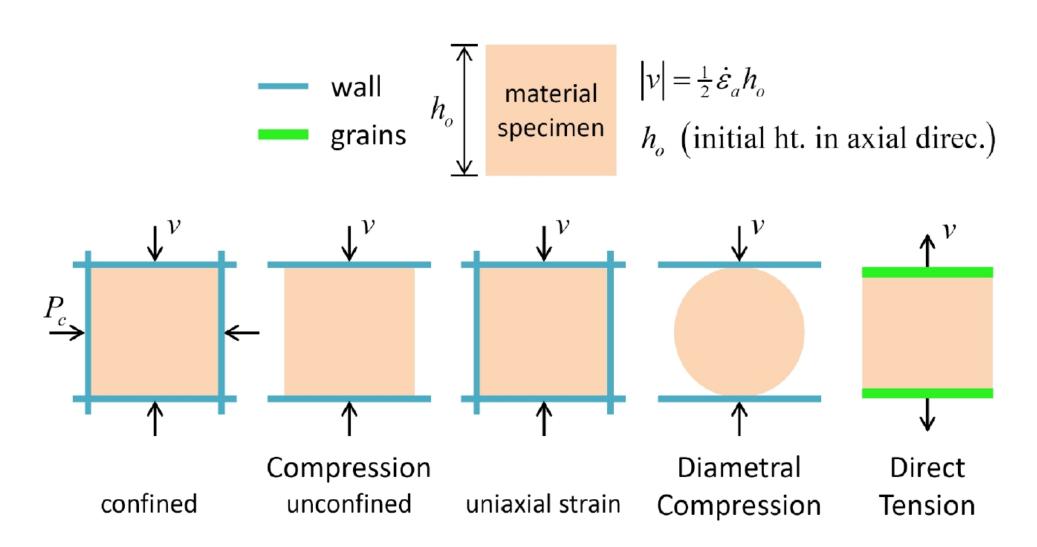
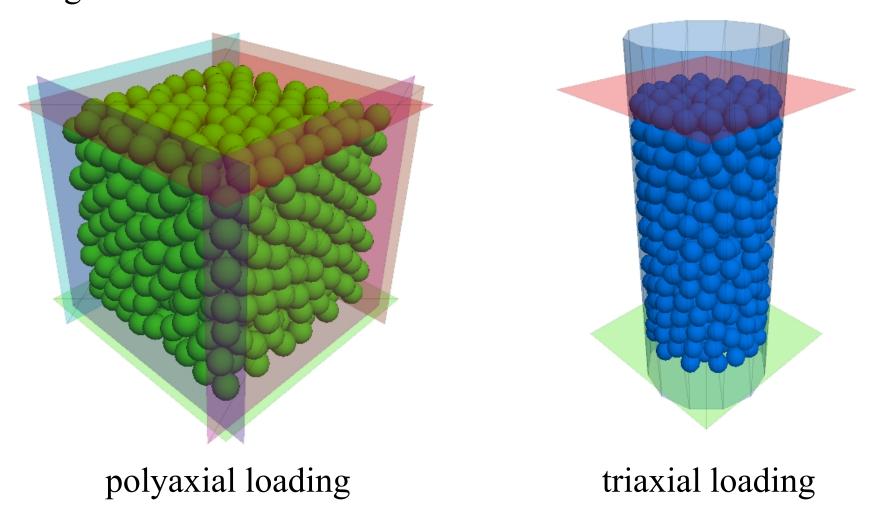


Figure 23 Loading conditions of laboratory-testing procedures.

Lab-Testing Procedures (compression test)

The axial walls act as loading platens, and the velocities of the radial walls are controlled by a servomechanism to maintain a constant confining stress.



Lab-Testing Procedures (compression test)

There is a seating phase followed by a loading phase.

Seating phase: strains reset to zero, confining pressure applied.

Loading phase: strains reset to zero, axial strain applied.

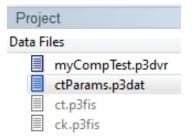
The loading phase may consist either of a single stage that ends when the applied deviatoric stress falls below a specified fraction of its peak value or multiple stages during which the axial-strain increments are specified.

During the test, the crack-monitoring package is on (for bonded materials), and specimen behavior is monitored using the history mechanism to store relevant quantities.

Lab-Testing Procedures (compression test)

Table 10 Compression-Test Parameters

Parameter	Туре	Range	Default	Description
Material-vessel param	eters ar	e listed in T	able 6.	
T, ct_testType	INT	{0,1,2}	0	test-type code 0, confined 1, unconfined 2, uniaxial strain
P_c , \mathtt{ct} _Pc	FLT	$\left(0.0,\infty\right)$	NA	confining pressure $(P_c > 0 \text{ is compression})$
$\dot{arepsilon}_a$, ct_eRate	FLT	$\big(0.0,\infty\big)$	NA	axial strain rate $(\nu = \frac{1}{2} \dot{\varepsilon}_a h_o, \ \dot{\varepsilon}_a > 0 \ , \ \text{see Figure 23}$ and Section 5.4)
C_l , $\mathtt{ct_loadCode}$	INT	{0,1}	0	loading-phase code
$lpha$, ct_loadFac	FLT	(0.0,1.0)	0.9	load-termination factor (C_l = 0) for termination criterion: $\left \sigma_d^w\right \leq \alpha \left \sigma_d^w\right _{\max}$
Servo-control group:				
$arepsilon_p, exttt{ct_PTol}$	FLT	$(0.0,\infty)$	pk_PTol	pressure tolerance $\left(\frac{\left P - P_c \right }{P_c} \le \mathcal{E}_{p} \right)$
$arepsilon_{ ext{lim}}$, $\mathtt{ct_ARatLimit}$	FLT	$(0.0, \infty)$	1×10^{-5}	where P is current pressure equilibrium-ratio limit (parameter of ft_eq)
$n_{ m lim}$, ct_stepLimit	INT	$\big[1,\infty\big)$	pk_stepLimit	step limit (parameter of ft_eq)
$v_{ m lim}$, ct_vLimit	FLT	$\big(0.0,\infty\big)$	$10H\dot{arepsilon}_a$	servo velocity limit (see Table 9)



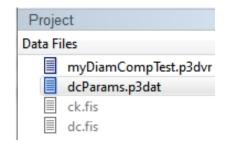
axial strain rate, must be slow enough to obtain quasi-static response

Lab-Testing Procs. (diametral-compression test)

The specimen is compressed between walls that act as loading platens while monitoring the wall-based axial force & displacement.

Table 11 Diametral-Compression Test Parameters

Parameter	Туре	Range	Default	Description
$\{w,d\}$, $dc_{w,d}$	FLT	$(0.0,\infty)$	NA	platen width and depth (2D model: $d \equiv 1$)
g,, dc_g0	FLT	$(0.0, \infty)$	NA	initial platen gap
E_p^* , dc_emod	FLT	$\big(0.0,\infty\big)$	mv_emod or NA	platen effective modulus (used by linear contact model)
$\dot{arepsilon}_a$, \mathtt{dc} _e \mathtt{Rate}	FLT	$\big(0.0,\infty\big)$	NA	axial strain rate $(v = \frac{1}{2}\dot{\varepsilon}_a g_o, \ \dot{\varepsilon}_a > 0, \ \text{see Figure 25}$ and Section 5.4)
C_l , $\mathtt{dc_loadCode}$	INT	{0,1}	0	loading-phase code { 0, single stage } 1, multiple stages
$lpha$, dc_loadFac	FLT	(0.0,1.0)	0.9	load-termination factor (C_l = 0) for termination criterion: $\left F_a\right \leq \alpha \left F_a\right _{\max}$
Static-equilibrium group:				
$arepsilon_{ ext{lim}}$, $ ext{dc_ARatLimit}$	FLT	$\big(0.0,\infty\big)$	1×10^{5}	equilibrium-ratio limit (parameter of ft_eq)
$lpha$, dc_stepLimit	INT	$\big[1.0,\infty\big)$	$\begin{array}{c} {\tt pk_stepLimit} \\ {\tt or} \ 2{\times}10^6 \end{array}$	step limit (parameter of ft_eq)



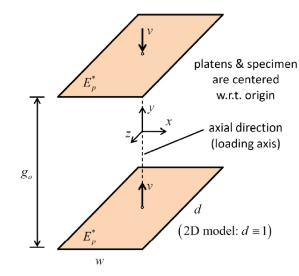


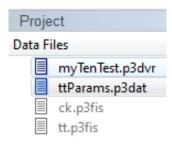
Figure 18 Loading configuration of diametral-compression test.

Lab-Testing Procedures (direct-tension test)

The specimen is gripped at its end (via grip grains) and pulled apart slowly while monitoring the axial stress and strain using the measurement-based quantities.

Table 12 Direct-Tension Test Parameters

Parameter	Туре	Range	Default	Description
Material-vessel para	Material-vessel parameters are listed in Table 6.			
t_{g} , tt_tg	FLT	$(0.0, \infty)$	0.1H	grip thickness
$\dot{arepsilon}_{_{\!a}}$, <code>tt_eRate</code>	FLT	$(0.0,\infty)$	NA	axial strain rate $(v = \frac{1}{2}\dot{\varepsilon}_a h_o, \ \dot{\varepsilon}_a > 0 \ , \text{ see Figure 17}$ and Section 5.4)
C_l , tt_loadCode	INT	{0,1}	0	loading-phase code { 0, single stage } 1, multiple stages
$lpha$, <code>tt_loadFac</code>	FLT	(0.0,1.0)	0.9	load-termination factor ($C_l = 0$) for termination criterion: $\left \sigma_a^m\right \leq \alpha \left \sigma_a^m\right _{\max}$



Specimen may have been created in physical vessel or carved out of a material block.

Example Materials

Each example serves as a base case, and provides a material at the lowest resolution sufficient to demonstrate system behavior. There is a material-genesis project for each material, and these projects are in the **fistPkgN/ExampleProjects/MatGen-M** directory. There are separate 2D and 3D projects for each material, and both projects are contained within the same example-project directory.

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When constructing a PFC material, start with the corresponding example project and modify it as necessary.

Clumped materials are created by calling mpParams-Clumped.p{2,3}dat.

1.1 Linear Material Example

The linear material example is in the MatGen-Linear example-project directory. A linear material is created to represent a typical aggregate base layer of an asphalt-surface roadway (Potyondy et al., 2016). We denote our aggregate material as the AG_Linear material with microproperties listed in Table 1. The material is created in a cylindrical material vessel (of initial 240-mm height and 170-mm diameter, with a 500 MPa effective modulus) and packed at a 150 kPa material pressure via the boundary-contraction packing procedure as shown in Figure 1. The material is then subjected to triaxial testing. During the triaxial test, the confinement is 150 kPa, and a load-unload cycle is performed at an axial strain of 0.05% to measure the resilient modulus (see Figure 2).² The hysteretic response is the expected behavior, and the resilient modulus is similar to the effective modulus of the linear material.

Table 1 Microproperties of AG_Linear Material

Property	Value		
Common group:			
N_{m}	AG_Linear		
T_m , α , C_ρ , $\rho_v \left[\text{kg/m}^3 \right]$	0, 0.7, 0, 2650		
$S_{g}, T_{SD}, \{D_{\{l,u\}} \text{ [mm]}, \phi\}, D_{mult}$	0, 0, {14,20,1.0}, 1.0		
Packing group:			
S_{RN}, P_{m} [kPa], $\varepsilon_{P}, \varepsilon_{lim}, n_{lim}$	10000, 150, 1×10^{-2} , 8×10^{-3} , 2×10^{6}		
C_p , n_c , μ_{CA} , v_{lim} [m/s]	0, 0.58, 0, 1.0		
Linear material group:			
E^* [MPa], κ^* , μ	500, 1.5, 0.4		

^{*} Linear material parameters are defined in Table 2 of the base memo.

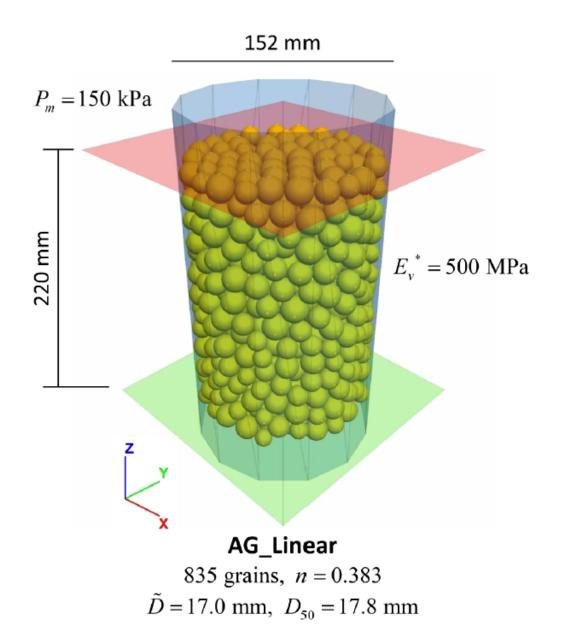


Figure 1 AG_Linear material packed at 150 kPa material pressure at the end of material genesis.

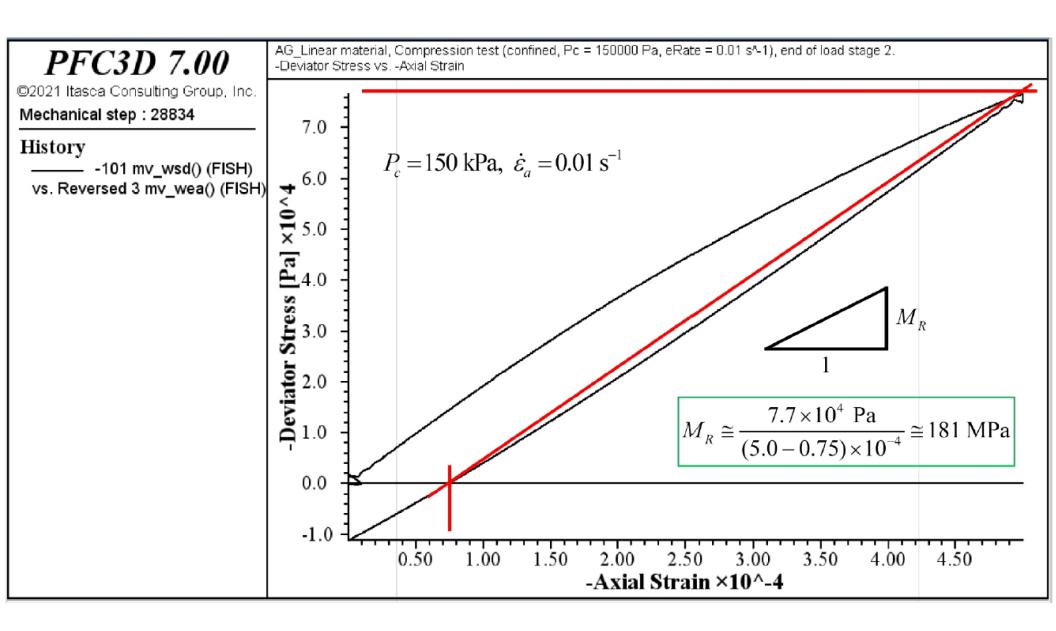


Figure 2 Deviator stress versus axial strain for AG_Linear material tested at 150 kPa confinement, and measurement of resilient modulus.

1.3 Contact-Bonded Material Example

The contact-bonded material example is in the MatGen-ContactBonded example-project directory. A contact-bonded material is created to represent a typical sandstone, which we take to be Castlegate sandstone. We denote our sandstone material as the SS_ContactBonded material with microproperties listed in Table 5. The material is created in a cubic material vessel (of 50 mm side length, with a 3 GPa effective modulus). The grain-scaling packing procedure is used to pack the grains to a 30 MPa material pressure, and then contact bonds are added between all grains that are in contact with one another (see Figure 11). The material is then subjected to compression, diametral-compression and direct-tension tests. The test results are shown in Figures 12–18.

⁴ The following properties are typical of Castlegate sandstone: density of 1960 kg/m³; median grain size of 0.19 mm; direct-tension strength of 1.0 MPa; unconfined-compressive strength of 20.0 MPa; and Young's modulus and Poisson's ratio measured during unconfined-compression test of 2.9 GPa and 0.33, respectively.

Table 5 Microproperties of SS_ContactBonded Material*

Property	Value		
Common group:			
N_m	SS_ContactBonded		
T_m , α , C_ρ , $\rho_v \left[\text{kg/m}^3 \right]$	1, 0.7, 1, 1960		
S_g , T_{SD} , $\left\{D_{\{l,u\}}\left[\text{min}\right], \phi\right\}$, D_{mult}	0, 0, {4.0,6.0,1.0}, 1.0		
Packing group:			
S_{RN}, P_m [MPa], ε_P , ε_{lim} , n_{lim}	10000, 30, 1×10^{-2} , 8×10^{-3} , 2×10^{6}		
C_p, n_c	1, 0.30		
Contact-bonded material group:			
Linear group:			
$E^*[GPa], \kappa^*, \mu$	3.0, 1.5, 0.4		
Contact-bond group:			
g_i [mm]	0		
$(T_{\sigma})_{\text{\{m, sd\}}}$ [MPa], $(S_{\sigma})_{\text{\{m, sd\}}}$ [MPa]	{1.0,0}, {20.0,0}		
Linear material group:			
E_n^* [GPa], κ_n^* , μ_n	3.0, 1.5, 0.4		

^{*} Contact-bonded material parameters are defined in Table 3 of the base memo.

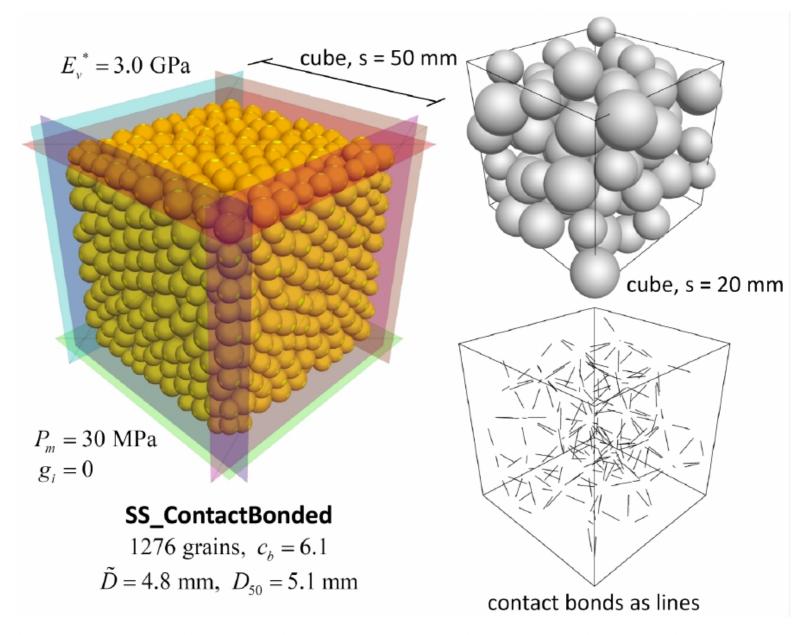


Figure 11 SS_ContactBonded material at the end of material genesis with grains and contact bonds in the microstructural box.

 $E_{v}^{*} = 3.0 \text{ GPa}$ $P_m = 30 \text{ MPa}$ $g_i = 0$

cube, s = 50 mm

Increasing the bond coordination number, increases the material modulus and strength.

> Bond coordination number is increased by either: increasing the material pressure, or increasing the installation gap.

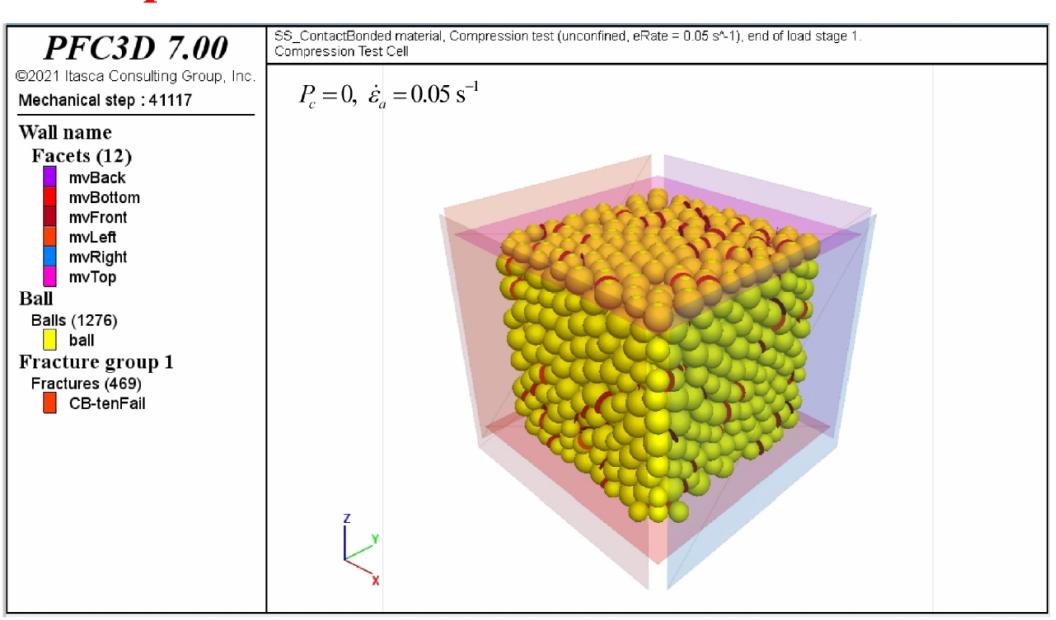


Figure 12 SS_ContactBonded material at the end of the fully unconfined test with grains and cracks.

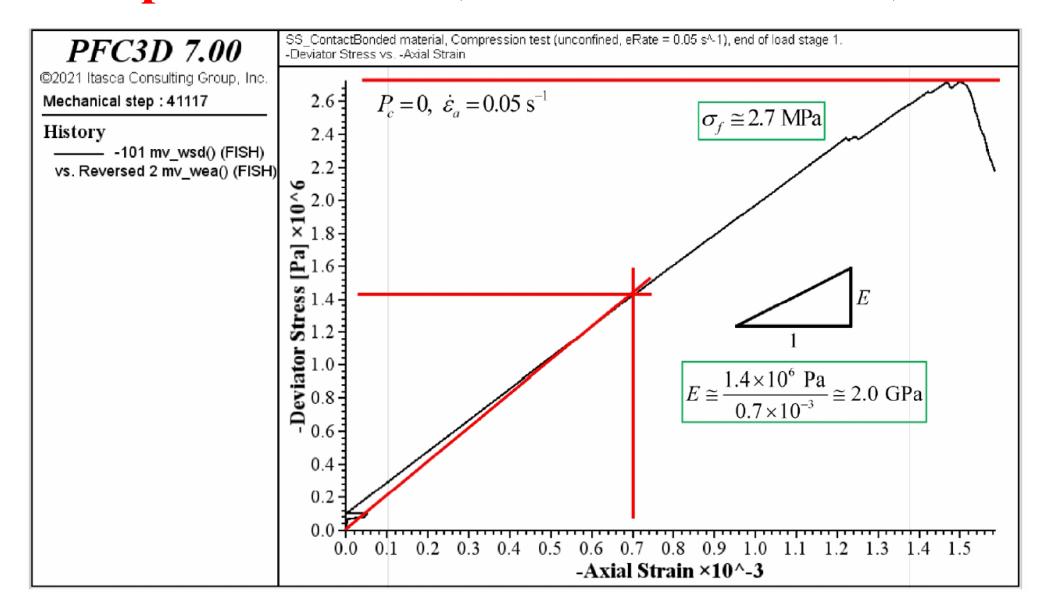


Figure 13 Deviator stress versus axial strain for SS_ContactBonded material tested fully unconfined, and measurement of peak strength and Young's modulus.

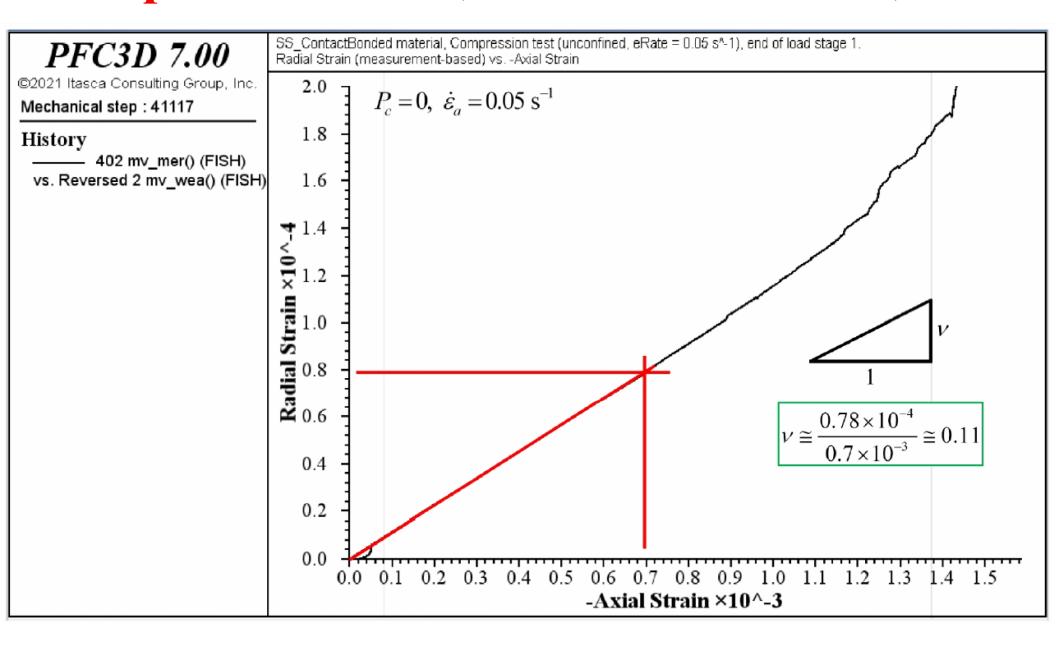


Figure 14 Radial strain versus axial strain for SS_ContactBonded material tested fully unconfined, and measurement of Poisson's ratio.

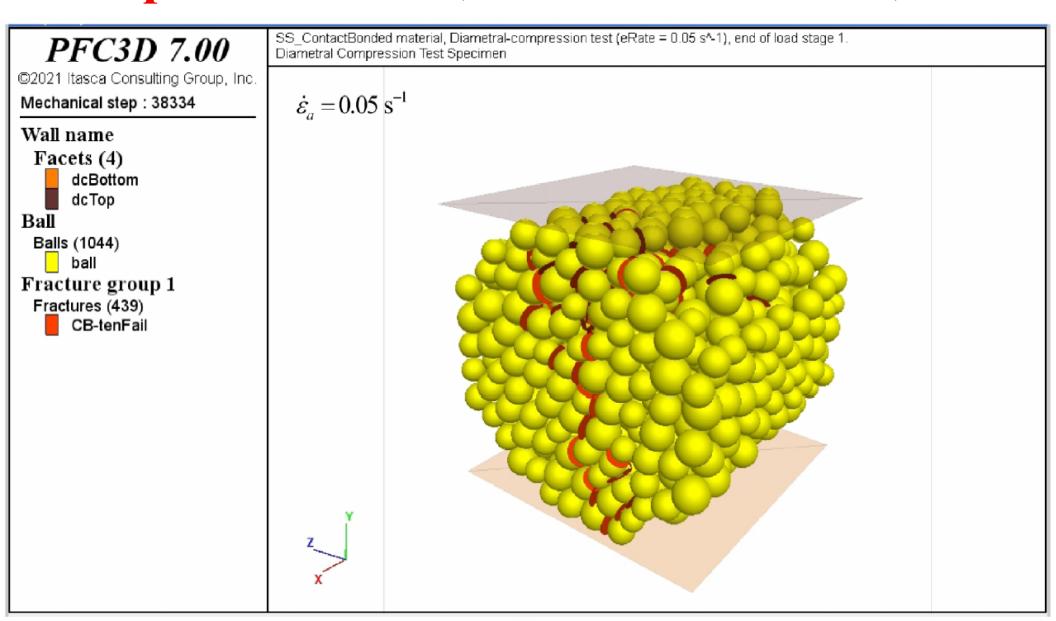


Figure 15 SS_ContactBonded material at the end of diametral-compression test with grains and cracks.

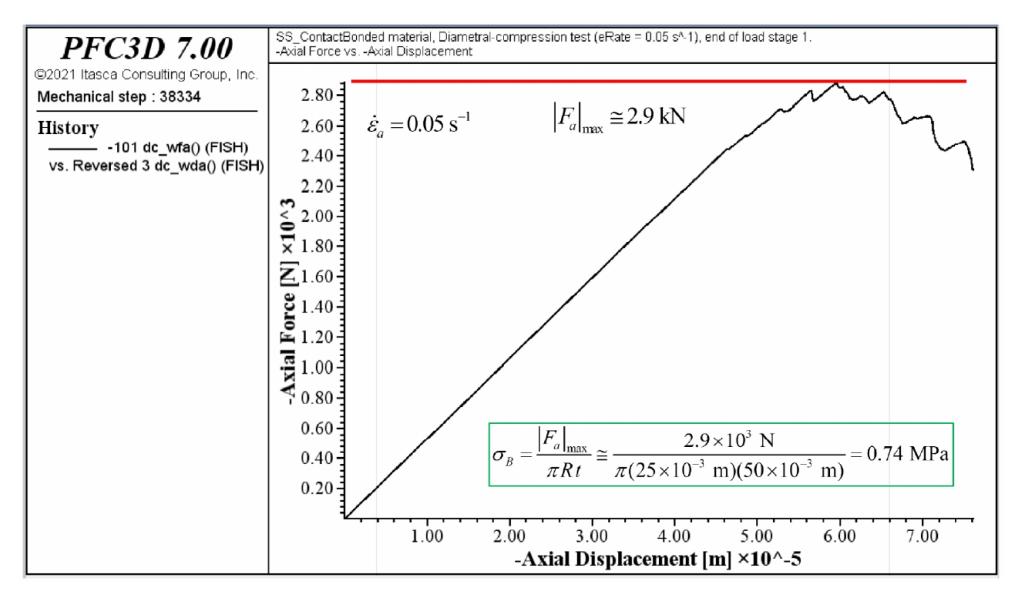


Figure 16 Axial force versus axial displacement for SS_ContactBonded material during the diametral-compression test, and measurement of Brazilian tensile strength.

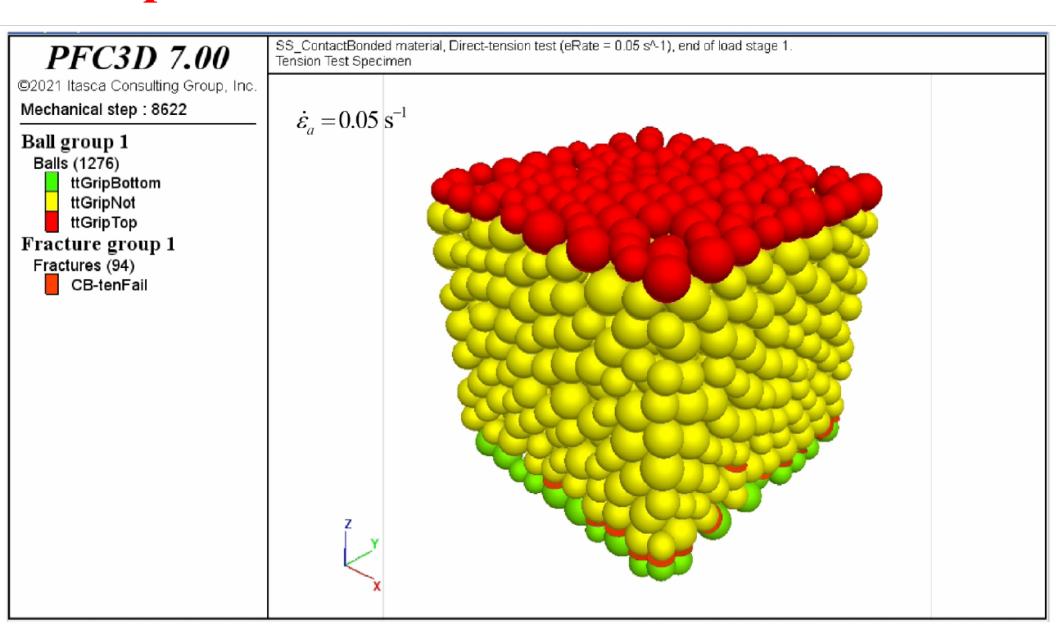


Figure 17 SS_ContactBonded material at the end of the direct-tension test with grains and cracks.

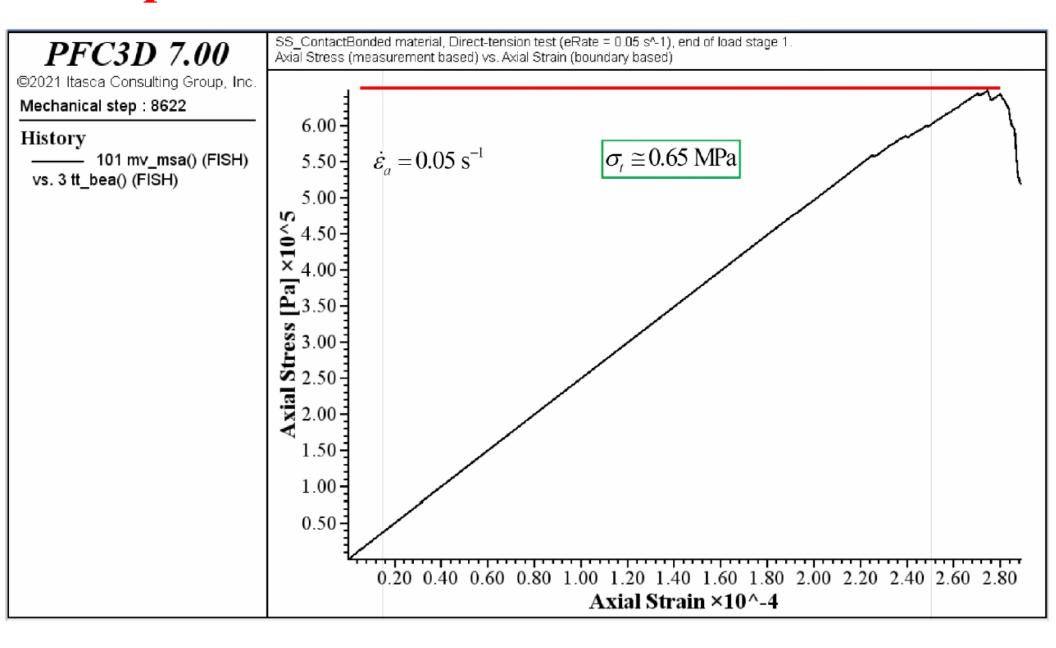


Figure 18 Axial stress versus axial strain for SS_ContactBonded material during the direct-tension test, and measurement of tensile strength.

Conclusion

The PFC model provides a synthetic material consisting of an assembly of rigid grains that interact at contacts. This synthetic material encompasses a vast microstructural space, and only a small portion of this space has been explored.

The PFC FISHTank provides a state of the art embodiment of four well-defined materials and a user-defined material to support:

- practical applications (via boundary-value models made from these materials), and
- scientific inquiry (via further exploration of this microstructural space).

Future Webinars

• Future webinars will introduce the BPM methodology, and discuss how to calibrate a BPM to match behavior of a particular rock.

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Stay tuned for more...

For now, calibration notes and material behavior:

Potyondy, D. (2018) "Calibration of the Flat-Jointed Material," PowerPoint Slide Set (April, 13, 2018).

Potyondy, D. (2021) "Flat-Jointed Material Behavior," PowerPoint Slide Set (June 21, 2021).